Mr. Pagle

FOR PALISADES RESERVOIR



U. S. ARMY ENGINEER DISTRICT, WALLA WALLA

CORPS OF ENGINEERS

NOVEMBER 1958

PALISADES DAM

JACKSON LAKE DAM

1953 Start contract

\$76,601,000

PALISADES RESERVOIR PERTINENT DATA

	FERTINENT	DATA	
Tota Join Mini I D Mini Dead Supe Supe Surf	RVOIR 1 Capacity at normal water surface t use storage space	App	. 1,200,000 ac.ft. . 200,000 ac.ft. . 155,500 ac.ft. . 44,100 ac.ft. . 5,497 m.s.l. . 5,452 m.s.l. rox. 16,000 ac.ft. . 5,621 m.s.l. rox. 16,000 acres
Type Volu Maxi Cres Cres Spil Comb su Sp Ou	ted on Snake Piver 7 miles upstream me	Approx. 14	olled earth fill ,000,000 cu. yds 260 feet 5,630 m.s.l 2,200 feet 5,570 m.s.l 90,000 c.f.s 47,000 c.f.s 29,000 c.f.s.
Inst Powe Powe Oper Tran	R PLANT alled capacity (4 Units at 28,500) r tunnel discharge capacity at mini rhouse, 132 ft. wide by 298 feet 10 ating head	imum power head ong by 113 feet h	10,000 c.f.s. igh 122 to 244 feet orming
Drai Drai Aver Maxi Mini Peak Mini Infl	DLOGY nage area above Heise, Idaho nage area upstream from Palisades : age annual runoff at Heise (1903-1) mum annual runoff at Heise (1956) mum annual runoff at Heise (1934) discharge of record at Heise (June mum discharge of record at Heise (ow design flood, volume 30 days . ow design flood, peak discharge .	Dam	5,110 sq.mi. . 5,047,000 ac.ft. 1/ . 6,523,000 ac.ft. . 2,881,600 ac.ft. . 51,600 c.f.s. 2/ . 1,210 c.f.s. . 3,320,000 ac.ft.
2/ P	unoff at Heise is 1-1/4 percent hi eak discharge of 60,000 c.f.s. occ ashing out of landslide on Gros Ve	urred May 19, 192	sades Dam. 7 as result of
	Irrigation Power Flood Control Fish and Wildlife Recreation nreimbursable	BENEFITS (Annual) \$1,981,000 1,604,000 899,330 7,940 252,300	REPAYMENT \$10,800,000 42,554,700 * *

 $\frac{\mathtt{COSTS}}{\mathtt{Total}} \hspace{0.1cm} \mathtt{project} \hspace{0.1cm} \mathtt{construction} \hspace{0.1cm} \mathtt{and} \hspace{0.1cm} \mathtt{development} \hspace{0.1cm} \mathtt{costs}$

JACKSON LAKE RESERVOIR

PERTINENT DATA

RESERVO IR	
	On Snake River about 25 miles north of Jackson, Wyoming and 1 mile west of Moran, Wyoming.
Surface area	847,000 ac.ft
Structural height . Hydraulic heights . Base width Crest width Altitude of crest . Volume Spillway type	Concrete gravity, embankment wings 70 feet 41 feet 61 feet 21 feet 4,920 feet 6,776.8 ft.(m.s.l.) 491,700 cu.yds. Overflow weir with 19 radial gates, each 8 feet by 6 feet 13,000 c.f.s.
OUTLET WORKS	
	6.5 feet
Capacity	
HYDROLOGY	
	at Moran (1904-1950) 1,020,000 ac.ft.

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8. Discharge entropy rettle - Shellow, Isalia

10. Third Carried Storage Renervation Diagram

C-1 Forecast Verification Analysis

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Cittly Discharge Hydrographs 1936 - 1955 - Sagles Liver on Series

SECTION I - INTRODUCTION

1.01 Authority. - This manual is prepared under authority contained in Section 7 of the Flood Control Act of 1944 (58 Stat. 890) which reads in part as follows:

"Hereafter, it shall be the duty of the Secretary of
War to prescribe regulations for the use of storage allocated for flood control or navigation at all reservoirs
constructed wholly or in part with Federal funds provided
on the basis of such purposes, and the operation of any
such project shall be in accordance with such regulations:"
General instructions regarding the preparation of the manual are

contained in Part CXXXVI, Reservoir Regulation, Engineering Manual,
Civil Works Construction, August 1951.

1.02 Purpose and scope. - Purpose of this manual is to present information for reference pertinent to system operation for flood control of Palisades Reservoir in conjunction with Jackson Lake Reservoir including details of facilities and regulation criteria. It contains a general description of the drainage basin and development. It describes the plan of operation, including regulation schedules for flood control, special regulation for unusual conditions and exceptionally large floods, and regulation examples. Comprehensive pertinent data are presented, including basin and reservoir maps, outlet and spillway discharge curves and tables, storage allocations, discharge rating tables for key stations, climatological data and hydrographs of stream flow at key stations for the period of record. The

organization and responsibilities of those concerned with proper operation of the projects are also included. The Bureau of Reclamation and Corps of Engineers in cooperation with other Federal and State agencies and private organizations, made extensive studies of water supply, bank protection and multiple-purpose water usage in the development of the operation plan. The degree of flood protection provided was determined from an analysis of flood records and historical data, with consideration given to present and future needs of irrigation and additional flood control storage facilities.

1.03 Revisions to this manual. - As a continuing program, it will be necessary to revise portions of this manual to keep it up to date. Pertinent discharge rating tables must be revised when changes become evident in the stage-discharge relation; likewise, changes in the plan of operation will be made for the purpose of improving regulation technique, and project developments may occur which require revision of the information presented in the manual. Whenever revisions are necessitated, new pages containing the revised material will be printed and issued to each person having a copy of the manual so that substitution may be made. Revised pages will show the date of revision.

SECTION II - DESCRIPTION OF DRAINAGE AREA

2.01 Topography and streams. - The drainage area above Palisades Dam is 5,110 square miles and is located in northwestern Wyoming and southeastern Idaho. The main stem of the Snake rises in the Rocky Mountains of Yellowstone National Park, Wyoming, from where it flows westerly in deep canyons or narrow valleys for approximately 35 miles to the junction of Lewis River, thence southerly into Jackson Lake Reservoir. From Jackson Lake the river flows southerly for about 50 miles through a flat valley known as Jackson Hole. At the lower end of Jackson Hole the river enters a canyon and gradually bends until it is flowing northwesterly as it crosses the Wyoming-Idaho border and into the upper end of Palisades Reservoir. Below Palisades Reservoir the Snake River continues to flow northwesterly through a narrow valley, emerging into Snake River plain over an alluvial fan and thence flowing southwesterly through highly developed irrigated areas and into American Falls reservoir. Regulation by Palisades effects most of its local flood benefits in the area between Palisades and American Falls. Tributaries to the Snake River above American Falls are generally mountain streams with steep slopes. The largest of the tributaries is Henrys Fork which has a drainage area of 3,280 square miles and enters, the Snake about 30 miles below Palisades. Pertinent data regarding the tributaries are given in the following table:

		Disch	narge in cfs	
Name	Drainage Area	Average Annual	Max. Year	Max. Peak
Henrys Fork	3,280	1,914	2,820	9,490
Blackfoot	1,295	159	294	868
Portneuf	1,000	259	414	2,000 +

A general plan of the area is shown on Plate 1.

- 2.02 Economy. The principal natural resource of the Upper Snake River area is the fertile agricultural land. Because of the shortness of the growing season in the valleys above Palisades Dam, the economy is based upon raising of cattle for beef and dairy farming on Salt River in Star Valley. In this area ranches engage in raising hay on all available valley floor lands for winter use to supplement upland summer range. Snake River plains below Palisades has developed into one of the most productive irrigated areas in the nation. At least 85 percent of the employment in the area is provided directly or indirectly by irrigated farms. Manufacturing is characterized by a preponderance of food processing plants, including sugar beet refineries, creameries, canneries, and meat packing establishments. Production of phosphate fertilizer and elemental phosphorus is of recent but increasing importance. Forestry, mining, and recreation are other industries of the area. The leading exports of the area are livestock, potatoes, sugar, beans, wool, grain, onions, and dairy products.
- 2.03 Irrigation. Because of the short growing season in the area above Palisades, irrigation of lands is not extensive being mostly confined to irrigation of pasture and hay lands. However, in the Snake River plain below Palisades, irrigation has reached a high degree of development. In this area the entire natural flows of all streams for many years have been diverted for irrigation use during July, August and September. During flood periods the diversion of flow for irrigation makes a substantial reduction in the magnitude of floods. Since 1920, expansion of storage facilities has been the chief irrigation development.

The following table shows average irrigation diversions from Snake River during the 10-year period 1944-53.

Irrigation diversions in 1,000 acre-feet

Month	Palisades to Shelley	Shelley to Blackfoot	Total	CFS
May	267.1	147.5	414.6	6,731
June	400.6	170.1	570.7	9,574
July	538.5	219.5	758.0	12,306
August	452.2	177.7	629.9	10,226
September	327.7	125.3	453.0	7,598

2.04 <u>Population</u>. - The population of the area above Palisades
Reservoir is 2,593 based on the 1950 census. The town of Jackson with
a population of about 1,200 is the largest community. In the area downstream of Palisades to American Falls there is a population of about
60,000. The principal towns with 1950 populations are as follows:

Pocatello	26,004
Idaho Falls	18,855
Rexburg	4,253
Blackfoot	5,178
American Falls	1,874

SECTION III - HYDROLOGY

- 3.01 Climate. Because of its geographic location, diversified topography, and wide range in elevation, the upper Snake River area has a variable climate ranging from semi-arid on the plains area below Palisades Dam to moderately wet on the west slopes of the Teton Mountains. Annual precipitation varies from less than ten inches in the plains area to a maximum of about 60 inches in the Teton Mountains. Characteristic of seasonal distribution is a May-June maximum occurring at lower elevations and a January maximum at higher elevations. July and August are uniformly the months of minimum precipitation. Much of the winter precipitation falls as snow. Mean monthly minimum and maximum temperatures in valley areas vary from 10.3 degrees to 86.0 degrees at Idaho Falls, Idaho, to minus 6.2 degrees and 76.4 degrees at Moran, Wyoming. Extreme temperatures vary from 104 at Idaho Falls to minus 63 degrees at Moran, Wyoming. Representative climatological data for the area are shown in Table 1.
- 3.02 Stream-flow characteristics. Snake River and its tributaries in the area have rather regular patterns of natural stream flow with high flows during the months of May through July, receding stream flow in August and September and low flows in the months of October through April. High flows in the late spring and early summer result from the melting of the winter-accumulated snow pack, sometimes augmented by runoff from rain storms. Maximum annual discharges usually occur as a result of above normal temperatures existing for a period of several days in succession. Daily discharge hydrographs for Snake River

at Moran are shown on Plate 6. Plates 7, 8 and 9 show daily discharge hydrographs for Snake River at Heise (Vince)

- upper Snake River area was that of 1894. No actual observations of discharge during this flood were made in the area, but estimates based on high-water marks and concurrent records in adjacent watersheds indicate a peak flow of approximately 65,000 cfs for the Snake River at Heise. The highest recorded discharge occurred in May 1927 and was the result of the failure of a landslide dam on Gros Ventre River. Approximately 50,000 acre-feet of water were released in a period of about three hours, resulting in a peak discharge of 60,000 cfs at Heise. Other large floods since 1902 were those of 1904, 1909, 1917 and 1918, with maximum discharges of 50,800, 44,000, 38,900 cfs and 52,000 cfs respectively. A tabulation of annual peak discharges and May-July volumes for the Snake River at Heise are given in Table 2. Tables 10 and 11 show the natural monthly volumes of runoff for period of record through 1950 at Moran and Heise.
- 3.04 Snake River channel capacity. The channel of the Snake River through Jackson Hole is generally inadequate to carry discharges of 8,000 cfs without appreciable damage from overflow and bank erosion. Below Palisades Dam the safe channel capacity varies from 15,000 cfs to 35,000 cfs. At 15,000 cfs, small areas, usually covered with natural pasture grass and which are annually subject to main river overflow, are inundated. For flows up to 20,000 cfs only pasture inundation occurs; however, some appreciable damage results from bank cutting. At the present time, levees constructed mainly by the Federal Government

protect areas lying along the Snake River from Heise to Henrys Fork for flows up to 30,000 cfs. Below Henrys Fork to American Falls, emergency works constructed by the Federal Government and local interests give a measure of protection to several critical locations.

3.05 Flood frequencies. - Frequency curves of maximum annual flood peak discharges for Snake River at Heise have been determined for actual conditions where flood control was incidental to regulation of Jackson Lake Reservoir for irrigation interests; for natural conditions approximating flows that would have occurred without regulation of Jackson Lake; and for conditions reflecting regulation of Palisades Reservoir and 200,000 acre-feet of storage space at Jackson Lake for flood control. Peak discharge data are available for Snake River at Heise for years 1903 to date. Frequency statistics for flood peak discharges were compiled and adjusted to the 97-year period of stream-flow records of Columbia River near The Dalles by methods described in Civil Works Engineer Bulletin 51-1 and subsequent publications by OCE on the subject of flood frequencies. Plate 2 depicts peak discharge frequency curves for Snake River at Heise, Idaho. The following tabulation briefly summarizes natural peak discharge magnitudes for various recurrence intervals.

Average recurrence interval	Maximum annual flo	od peak discharge
	<u>Natural</u>	Regulated
Years	c.f.s.	c.f.s.
2	32,500	20,000
5	42,300	21,000
10	48,700	21,900
20	54,500	23,000
50	62,000	25,800
100	68,000	29,800

3.06 Flood damages. - Flood damages in the region are mostly to agricultural lands and produce. Without the advantage of flood-control storage facilities the average annual damages along the Snake River from Palisades Dam to American Falls are estimated at \$2,700,000. Operation of Palisades Reservoir and Jackson Lake as outlined in this manual is expected to reduce average annual damages by about \$1,350,000. Plate 3 shows the average relationship of flood damages to peak discharges. The use of space in Jackson Lake in conjunction with Palisades space for flood control purposes also provides a reduction of flood damages in the Jackson Hole area between Jackson Lake and Palisades Dams.

In addition to the reduction of flood damages in the upper reaches of the Snake River, regulation by Palisades will be effective in reducing damages along the lower reaches of the Snake and along the lower Columbia River. The main control plan for control of floods on the lower Columbia River includes Palisades in the system of flood control reservoirs.

liant is effected by two redistrictions and by 50 fact units

SECTION IV - PROJECT DESCRIPTIONS

4.01 Palisades Dam. - Located on Snake River seven miles upstream from Irwin, Idaho, was authorized for construction by the Secretary of Interior on 9 December 1941 under provisions of Section 9 of the Reclamation Project Act of 1939. Reauthorization was made by Public Law 864, 81st Congress, 2nd Session; approved 30 September 1950. The total storage capacity of the reservoir at normal water surface is 1,401,600 acre-feet. Of the total storage, 1,200,000 acre-feet are allocated for joint use of irrigation, flood control, and production of power; 155,500 acre-feet are inactive storage for power head and for preservation and propagation of fish and wildlife; and 44,100 acre-feet are dead storage. Construction of Palisades Dam was started in 1951 and completed in 1957. The general plan and sections of the dam are shown on Plate 4. Table 3 shows capacity of the reservoir at one foot elevation increments. spillway is a tunnel, located in the left abutment and designed to discharge 47,000 cfs at normal water surface elevation. Control of the spillway is effected by two radial regulating gates, 20 by 50 feet each. The tunnel is 1,890 feet long and, except for inlet and outlet ends, lined with unreinforced concrete. The outlet works consist of a trashrack structure, two circular tunnels with steel liners downstream from the dam axis, manifold section, valve house, and stilling basin. The two tunnels, one power and one outlet with diameters of 26 feet, have a total capacity of 32,500 cfs at minimum power pool elevation of 5,497.5 feet m.s.1.; 10,000 cfs through the power tunnel and 22,500 cfs through the outlet tunnel at minimum power head. The outlet tunnel has

six discharge tubes for control of irrigation and flood water. The power tunnel has two bypass tubes for routing floods and four penstocks for generation of power. There are four regulating gates, four emergency gates, two 96-inch hollow jet valves and two 96-inch ring follower gates for control of the outlet tunnel discharge, and two regulating and two emergency gates for control of the power tunnel bypasses. The regulating gates are hydraulically operated 7 foot-6 inch by 9 foot-0 inch rectangular gates. Spillway and outlet discharge curves are shown on Plate 4. Pertinent data are summarized in the table at the forepart of this manual.

4.02 Jackson Lake Dam. - Jackson Lake Dam is located on Snake River in the State of Wyoming and controls the outflow from Jackson Lake. Originally, in 1907, the reservoir was formed by a temporary log crib dam creating a usable capacity of 300,000 acre-feet. This dam washed out in July 1910 and was replaced by an earth dam, forming a reservoir with a usable capacity of 380,000 acre-feet. The earth dam was raised in 1916, increasing the usable capacity to 780,000 acre-feet. In 1919, the capacity was further increased to 847,000 acre-feet between elevations 6,730 and 6,769 m.s.l. by dredging the outlet. The reservoir covers an area of about 25,540 acres. Table 4 is a storage capacity table for Jackson Lake. The spillway dam is a concrete gravity type with embankment wings having a structural height of 70 feet and hydraulic height of 41 feet. The spillway is an overflow weir controlled by 19 radial gates, 8 feet by 6 feet each with a total capacity of 13,000 cfs. The outlet works consist of 20 slide gates, 8 feet by 6.5 feet each, having a total capacity of 15,000 cfs. The general plan and sections of the dam are shown on Plate 5. Pertinent data are summarized in a table at the forepart of this manual.

SECTION V - PLAN OF OPERATION

5.01 History of plan of operation. - A draft of the plan of operation for Palisades Reservoir was prepared by the Bureau of Reclamation in cooperation with the Portland District, Corps of Engineers, and submitted to the Chief of Engineers in January 1948, along with a report on the derivation of the operation plan showing estimates of flood control benefits. The Office, Chief of Engineers concurred with estimates of flood control benefits expected to accrue from proposed plan of operation, and informed the Commissioner, Bureau of Reclamation by letter dated 28 January 1948 that, upon completion of the structure, recommendations of the Chief of Engineers to the Secretary of the Army for regulation under Section 7 of the 1944 Flood Control Act would be in accordance with the allocation for flood control as contained in the adopted plan of operation. Copies of the operation plan as prepared in 1948 were attached to contract with water user organizations for use of Palisades water. It was included as an appendix to the Bureau of Reclamation supplemental report on Palisades Dam and Reservoir Report, dated June 1949, which was basic to final authorization of that project. Also it was contained in the Definite Plan Report for Palisades Reservoir prepared by the Bureau of Reclamation and dated November 1951. Appendix A is a copy of this operating plan.

Recent studies have indicated some improvement and interpretations to the plan. The following items have been agreed to by exchange of letters between the Corps of Engineers and the Bureau of Reclamation:

- a. That the best available forecasts be adopted, regardless of the basis upon which they were made.
- b. That the wording of the Original Operating Plan be interpreted to provide for the development and maintenance of an adequate hydrologic reporting network.
- c. That numbered paragraph 2 of the Original Operating Plan is broad enough to accommodate the power plant operations relative to and consistent with the flood-control evacuation program.

In accordance with Federal law the regulations were summarized for publication in the Federal Register. This summary of regulations which includes the revisions mentioned above is included as Appendix B to this manual.

- 5.02 Essential features of plan of operation. The operation plan provides for the optimum feasible use of the storage space in Palisades Reservoir for flood control in coordination with its uses for irrigation, power and recreation, and in coordination with use of storage in Jackson Lake. Salient features of the plan are summarized as follows:
- a. Storage space up to 1,400,000 acre-feet in Palisades and

 Jackson Lake will be made available for flood control on a forecast basis

 by the Bureau of Reclamation in accordance with Flood Control Storage

 Reservation Diagram shown on Plate 10. However, not less than 75 percent

 of total storage space required at any time will be made available in

 Palisades Reservoir.
- b. Forecasts of runoff volume from forecast date until 31 July for operation of reservoir will be made periodically beginning 1 February by Bureau of Reclamation, Region I after consultation with U. S. Army Engineer District, Walla Walla, and Idaho State Watermaster District 36.

- c. Reservoir releases will be scheduled to evacuate and refill reservoir space in accordance with Flood Control Storage Reservation

 Diagram without exceeding 20,000 cfs at the Heise gaging station insofar as practicable.
- d. For extraordinarily large floods which require more than 1,400,000 acre-feet in Palisades and Jackson Lake to regulate flow to 20,000 cfs at Heise, releases in excess of 20,000 cfs will be planned as given in paragraph 5.05.
- e. When the forecasted runoff for the period 1 June through 31 July exceeds 2,500,000 acre-feet, and when, after 1 June, the available space is not within 10,000 acre-feet of the space required by the Flood Control Storage Reservation Diagram, the releases from the reservoir may be increased so that the flow at Heise will exceed 20,000 cfs up to a limit of 30,000 cfs to the extent of 1,000 cfs for each 5,000 acre-feet of deficient storage space, except that the release shall not be greater than natural inflow. The change in discharge will be made in such manner as to minimize the adverse downstream effects.
- f. A hydrologic reporting netowrk sufficient to provide the necessary basic data for determination of required flood control reservation shall be developed and maintained by the Bureau of Reclamation.
- g. Current information on forecasts, reservoir releases, reservoir storage and such other operating criteria which affect the schedule of operation shall be furnished the District Engineer, Corps of Engineers and Watermaster, Water District No. 36, by the Bureau of Reclamation.

- plan depend to a great extent on the adequacy of the runoff forecasts.

 Because runoff above Palisades Dam is primarily from melting of the accumulated winter and spring snow pack, forecasts of runoff volume can be made with a reasonable degree of accuracy. In accordance with the operating plan, the Bureau of Reclamation will make forecasts of seasonal volume runoff for operation of reservoirs periodically commencing with 1 February of each year after consultation with Corps of Engineers and State Watermaster District 36. The forecasting equations developed by the Bureau are included as Appendix C to this manual. They consist of statistically derived relationships of past occurrences of runoff and snow fall, precipitation, and temperature. Results of the forecasts as would have occurred in past years are also shown on Table C-1 of Appendix C. Plate C-1 shows probability levels for various magnitudes of forecast errors.
- 5.04 Derivation of storage reservation diagram. The allocation of flood control storage space in the reservoirs is based on a storage reservation diagram shown on Plate 10. This diagram was developed by enveloping points relating the volumes of flood season runoff with coordinates of time and storage reservation required for control of the floods. Analysis of past floods provide the points from which the curves were drawn. Flood season runoff for each year of record was analyzed for the amount of storage reservation that would be required to control the runoff to the allowable discharge in Snake River channel at the Heise gaging station. This value is defined as bankfull capacity in the main channel below Palisades Dam (20,000 cfs). The values of

storage reservation required were plotted on the date the storage would be required and, adjacent to each plotted point, the runoff from that date to 31 July was noted. Curves were sketched as enveloping lines which encompassed the maximum required storage reservation on any date for any of the floods studied. In addition to enveloping the points of maximum storage requirements, the curves were shifted so as to provide increasing amounts for an additional safety factor in the early part of the season, prior to 1 June. Curves as originally developed are shown on Plate A-1 of Appendix A. Subsequent studies indicated a need for modifying the curves as applicable to low runoff years to insure refilling of the reservoir. Accordingly, the curves were modified to provide greater assurance of filling and still provide required flood control space by construction of two sets of curves; one set to be used until natural inflow to Palisades first exceeds 20,000 cfs and the other set to be used after that time. The curves are shown on Plate 10, and Plate B-1 of Appendix B.

5.05 Regulation of extraordinary large floods. - Although most floods can be regulated to bankfull by use of the storage reservation diagram, Snake River is occasionally subjected to floods much larger which cannot be so regulated. With present downstream channel capacity, there is insufficient reservoir capacity to regulate the standard project flood and maximum historical floods to bankfull. Also, heavy precipitation and consequent snow accumulation may develop late in the season, leaving insufficient time to evacuate the reservoir to obtain required space for regulation to bankfull. For these floods, operation of the reservoir to permit releases above bankfull will materially

reduce the magnitude of the peak discharge downstream. These extraordinarily large floods are expected to occur very rarely. The rate of releases from Palisades and Jackson Lake Dams for such floods will be determined in accordance with the following rule curve showing the relationship of required discharge to the 1 May - 31 July forecast of runoff volume:

1 May - 31	July Forecasted Volume	Required Discharge 1/
e de transce	(acre-feet)	(cfs)
Less than	4,100,000	20,000
	4,100,000	23,000
	4,300,000	24,000
	4,600,000	25,000
	4,900,000	26,000
yt 11 -	5,300,000	27,000
DOE LANG SE	5,600,000	28,000
	6,000,000	29,000
	6,300,000 or larger	

1/ Applicable only when exceeded by natural inflow to Palisades Reservoir.

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Releases of the above amounts begun in May will be modified after

1 June in accordance with the procedure set forth in 5.02e. Regulation
of the Standard Project Flood as would occur by this plan is shown on
Plate 11. Regulation of the 1953 flood is shown on Plate 12.

5.06 Regulation for power production. - As an integral part of the Palisades Project, a power plant has been constructed with an installed capacity in four units totalling 114,000 kilowatts. The power plant is designed to operate through a range of head varying from a minimum of 122 feet to a maximum of full reservoir of approximately 245 feet. Use of water for power production will be limited to water released for irrigation or flood control purposes including release of water to fill the prior storage right of American Falls Reservoir. The normal

production of hydroelectric power at Palisades Dam will be incidental to the operation of the reservoir for irrigation and flood control. There are no power-generating facilities in operation at Jackson Lake Dam.

- 5.07 Continuing and additional operation studies. In the interest of obtaining maximum benefits from the operation of the reservoir, a program of continuous study of each current flood for possible improvements in the regulation schedules will be necessary at all times. Some of the continuing and additional studies are enumerated as follows:
- a. Review runoff forecasting techniques with a view toward gaining greater accuracy.
- b. Analysis of recent and current data to determine what additional data are required for improvement in forecasting.
- c. Studies to determine a reliable method of forecasting short-term stream flows.
 - d. Review of Storage Reservation Diagram.
- e. Review of basis for releases in expess of 20,000 cfs when required for control of extraordinary large floods.
- f. Studies to provide for better integration of Palisades
 Reservoir into the entire Upper Snake water control system, including
 all irrigation and storage features above American Falls Dam.

SECTION VI - COLLECTION OF DATA AND COMMUNICATION

- 6.01 <u>General</u>. It is essential for efficient regulation of the reservoir that those responsible for regulation keep advised of weather, snow pack, and stream flow conditions within the watershed, and also informed regarding current storage in the reservoirs. Facilities for gathering and transmitting this information are discussed in the following paragraphs.
- 6.02 Hydrologic reporting network. The hydrologic network in the upper Snake River drainage basin for operation of the reservoirs in the interest of both irrigation and flood control consists of three reservoirstage stations, five stream-flow stations, seven precipitation stations and 33 snow courses. Locations of stations in the Hydrologic Network are shown on Plate 1. All the precipitation network stations are equipped with manual-type gages; however, two stations, Moran and Jackson, are also equipped with recording gages. Reports received from the Hydrologic Network may be divided into two groups; those received daily for shortterm stream flow forecasting and project regulation during the spring runoff period, and those received monthly or semimonthly primarily for forecasting seasonal volume of runoff. Tables on Plate 1 list snow courses, stream and reservoir stations and precipitation gages together with the period, frequency, and method of reporting. Table 5 shows representative snow course data. Discharge rating tables for stream gaging stations are included as Tables 6, 7, 8 and 9.

As indicated on Plate 1, nearly all of the required daily reports are received at the Corps of Engineers' District office by Teletype

Service "C". Reports used for daily forecasts of stream flow as well as daily reservoir reports are received daily during the flood season,

1 April through 15 July. The Minidoka Project Office at Burley will collect the reports from most of the local observers by telephone, mail, and radio; transmitting them each morning to the U. S. Weather Bureau at Boise, from where they are transmitted by Teletype Service "C". Precipitation reports from Snake River Station, Jackson, Island Park and Moran will be collected through the Bureau of Reclamation operator at Jackson Lake and relayed to Burley, together with reservoir and stream flow observations through the Palisades Project. The cooperative observers at Bedford and Grover will report daily precipitation amounts in excess of 0.20 inch by telephone directly to Burley. For lesser daily amounts of precipitation the reports will be forwarded to Burley by mail.

Monthly and semimonthly reports of snow conditions in the upper watershed are obtained by the Soil Conservation Service in cooperation with the Bureau of Reclamation, the Corps of Engineers, the Forest Service, Water District No. 26, and the States of Wyoming and Idaho. These reports are transmitted to the District Engineer in accordance with the schedule shown on Plate 1.

Daily precipitation, temperature, reservoir stages and outflows are observed by the operators at Island Park, Jackson Lake and Palisades Reservoirs and transmitted by radio (telephoned from Palisades) to the Bureau of Reclamation's Minidoka Project office at Burley and thence by teletype, during the period 1 April through 15 July, to the U. S. Weather Bureau office at Boise for transmission over Teletype Service "C". Daily stream-flow reports of Wilson, Heise, and Rexburg are telegraphed by the

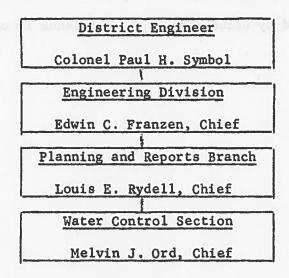
observers, during the 1 April through 15 July period, to the Weather
Bureau at Boise for transmission by Teletype Service "C". The reservoir
outflows and stream-flow data are from rated stream-gaging stations.

During the 15 July through 31 March period, no daily reservoir or
stream-flow reports are received by the District Engineer, but a weekly
report showing daily flows at gaging stations and periodic observations
of reservoir stages is received by mail from the Watermaster of District
No. 36 at Idaho Falls.

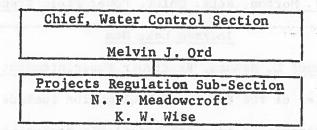
6.03 <u>Communication facilities</u>. - As indicated in the foregoing paragraphs, use is made of all types of communication facilities in the collection and dissemination of hydrologic data and exchange of regulation requirements. Normal use was adopted for that facility which gave dependability and was most economical. Duplication of reporting requirements was avoided wherever practical, and use of more costly communication service was avoided where the data are not material in the determination of immediate operation requirements. Improvements and economics will be effected as indicated by accumulation of experience in operation of the network.

SECTION VII - ORGANIZATION AND RESPONSIBILITIES

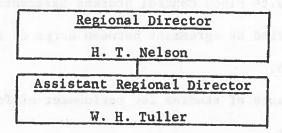
- 7.01 General. The various interests affected by regulation of Palisades and Jackson Lake Reservoirs demand close cooperation among the Corps of Engineers, Bureau of Reclamation and Reclamation Engineer for State of Idaho. The administration of regulating programs will at all times reflect due consideration for the integrated interests involved. The organization and responsibility of these agencies as they relate to the operation of Palisades are given in the following paragraphs.
- 7.02 Corps of Engineers. The Army Engineer District, Walla Walla of the Corps of Engineers has the responsibility of prescribing flood control regulations in accordance with Section 7 of the Flood Control Act of 1944 as referred to in paragraph 1.01. Within the District, the Engineering Division is responsible for conformance with Section 7 with primary responsibility assigned to the Water Control Section. The organization of the District as it pertains to flood control regulations is as follows:

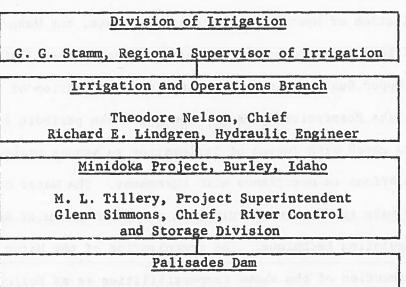


By collection of hydrologic and reservoir data, the Water Control Section will keep informed on the hydrological and meteorological situation in the Upper Snake drainage area and in the operation of Palisades and Jackson Lake Reservoirs. The Section will make periodic forecasts of runoff and check with Bureau of Reclamation to assure maximum flood control regulations in accordance with agreement. The Water Control Section will make studies in coordination with the Bureau of Reclamation to refine regulation technique. The organization of the Water Control Section in execution of the above responsibilities is as follows:



7.03 <u>Bureau of Reclamation</u>. - The Regional Office, Region 1,
Bureau of Reclamation in Boise, Idaho, is directly responsible for the
operation of Palisades and coordination of Palisades' operations with
that of Jackson Lake to accomplish the flood control objectives. These
objectives will at all times be in accordance with regulations set forth
in the plan of agreement as given in Appendix A and B to this manual.
The organization of the Bureau of Reclamation as it pertains to the
operation of these projects is as follows:





B. J. Morton, Actg. Chief, Power Field Branch

Jackson Lake Dam

James L. Braman, Reservoir Superintendent

The responsibilities of the Bureau of Reclamation include the following:

- a. Maintenance of adequate hydrologic reporting network;
- b. Collection and dissemination of hydrologic and reservoir data;
- c. Preparation of periodic forecasts of runoff for the period February through July and consultations with the Corps of Engineers and District Watermaster to coordinate forecasts and establish details of the flood control evacuation and refill schedules.
- d. Execution of releases at Palisades and Jackson Lake as required to conform with Flood Control Storage Reservation Diagram or as these may be modified by agreement between Corps of Engineers and Bureau of Reclamation.
- e. Performance of studies for refinement of forecasting and regulation techniques.

The coordination of the foregoing responsibilities will be carried on by Mr. Richard E. Lindgren, acting directly under the Assistant Regional Director, W. H. Tuller, who is directly responsible for the operation of all Bureau of Reclamation reservoirs in Region 1.

7.04 Reclamation Engineer. - The Watermaster for the Upper Snake River District is the representative for the locality of the Idaho State Reclamation Engineer. He is elected by the water users holding adjudicated rights and is responsible for the distribution of the waters of Snake River in accordance with established water rights. The Watermaster is also responsible for the functional regulation of Jackson Lake for flood control in accordance with existing agreements and in coordination with the flood control activities at Palisades. In this capacity, the Watermaster each year makes periodic forecasts of the runoff of Snake River which will be correlated with those made by the Bureau of Reclamation. The present Watermaster is Lynn Crandall and has his office in Idaho Falls, Idaho.

The constantion of the levelegang responsibilities will be invited on the servers of the by Mr. Blacket S. Lindgern, driving directly appear the servers of the court director, w. W. Initer, who to directly responsible to the servers of all params of Sections of Sections

The Manager for the Companies of the Manager for the Upper State at the District to the Children State and District to the Companies of the Companies of the Companies of the Companies of the Manager for the

TABLE 1
CLIMATOLOGICAL DATA

(Snake River Basin above Idaho Falls, Idaho)

				Temper	Temperature-Degr	ee	Fahrenheit	Annual	Precipitation	in	Inches	Snowfall-Inches	l-Inches
Station	Watershed	Elev.	Period of Record	Years of Record	Mean	Highest of Record	Lowest of Record	Years of Record	Average	Maximum	Minimum	Years of Record	Average Annual
Afton, Wyoming	Salt River	6,225	1904-1946	34	38.0	98	-55	32	17.63	26.41	12.35	37	90.1
Alta, Wyoming	Henrys Fk.	6,500	1910-1954	43	39.1	97	-46	#	18.23	28.02	9.47	38	100.0
Bechler River, Wyoming Snake River 6,300	Snake River	6,300	1931-1944	10	38.7	96	_47	13	36.90	48.89	10.06	12	297.7
Bedford, Wyoming	Salt River	6,221	1902-1954	46	38.5	100	94-	42	19.46	29.71	10.78	47	107.1
Jackson, Wyoming	Snake River	6,244	1905-1954	32	37.7	96	-52	30	15.94	21.47	10.93	25	82.3
Moose, Wyoming	Snake River	6,627	1936-1954	18	36.2	92	+++	19	26.89	32.94	17.70	12	177.6
Moran, Wyoming	Snake River	River 6,740	1911-1954	42	34.2	92	-63	42	21.36	29.32	13.51	35	134.9
Snake Riv.Sta., Wyoming	Snake River 6,800	6,800	1906-1954	35	34.7	97	-56	32	30.13	50.10	21.32	35	208.3
Ashton, Idaho	Henrys Fk.	5,100	1897-1954	56	41.3	100	-37	53	16.37	24.18	8.97	47	72.5
Idaho Falls, Idaho	Snake River 4,744	4,744	1880-1954	50	9* 44	104	-37	63	11.31	21.31	5.93	49	и4.2
Irwin, Idaho	Snake River 5,200	5,200	1894-1954	51	41.8	102	-45	57	14.85	24.33	4.75	43	63.2
Island Park, Idaho	Henrys Fork	Fork 6,300	1942-1954	12	36.7	91	-60	12	30.27	37.43	24.15	5	179.0
Lake, Idaho	Henrys Fork	6,700	1890-1945	2	38.8	92	-39	22	17.65	22.35	11.93	15	132.2
Sugar, Idaho	Henrys Fork	Fork 4,892	1907-1954	35	41.6	104	-44	94	11.02	19.24	6.52	33	46.9
Grover, Wyoming	Salt River	6,115	1904-1952	45	37.7	96	-55	49	18.04	26.41	12.35	38	88.6

TABLE 2

RUNOFF AND DISCHARGE DATA

SNAKE RIVER NEAR HEISE, IDAHO

SNAKE RIVER AT MORAN, WYO.

	Annual	Actual 1	Natural	Natural	ſ		Natural	Natural_
	OctSept.	peak	Peak	May-July			Peak	May-July
Year	Runoff		Discharge	Volume		Year	Discharge	Volume
	1,000 A.F.		1,000 cfs	1,000 A.F.			1,000 cfs	1,000 A.F.
1903		23.0	32.0					
04	6,573	49.5	52.2	4,275		1904	8.2	885
	2.083	13.5	18.3	1,756		05	5.0	467
1905	2,983			2,753		06	6.0	591
06	4,095	19.0	27.0			07	7.6	894
07	5,922	23.5	32.4	4,290	W I	08	6.4	560
08	5,061	18.5	26.5	2,645	7.		14.2	814
09	6,911	44.0	48.7	4,600		09		881
1910	5,599	22.0	30.9	2,862		1910	10.1	
11	5 ,7 58	32.6	40.6	3,633		11	13.3	981
12	5,949	39.3	45.6	3,806		12	12.2	808
13	6,442	30.5	38.9	3,787		13	14.7	968
14	5,809	26.0	35.0	3,384		14	12.5	749
1915	3,940	17.1	19.5	1,742		1915	6.9	408
16	5,761	28.1	36.8	3,477		16	13.5	874
17	6,448	38.9	39.5	3,140		17	13.0	880
18	6,620	52.0	54.2	4,014		18	17.0	921
19	3,869	17.9	24.1	1,635		19	7.2	417
1920	5,082	26.0	35.0	3,348		1920	9.2	693
21	5,690	34.0	40.5	3,545		21	10.0	756
22	5,129	26.3	33.9	3,196		22	10.0	716
23		24.5	33.1	3,007		23	9.0	677
24	3,766	15.4	20.6	1,831		24	5.9	430
1925		25.1	35.7	- 3,542		1925	12.9	924
26		19.0	20.4	1,722		26	9.5	465
27	5,782	36.0	41.5	4,079		27	14.2	1,038
28	6,195	36.1	44.0	3,793		28	15.2	984
		24.3	29.6	2,355		29	9.0	578
29			24.1	2,143		1930	6.4	493
1930		20.5	14.8	1,264		31	4.6	344
31	3,231	12.6				32	9.6	718
32		21.3	30.5	2,942		33	10.3	620
33	4,323	25.6	31.5	2,358		34	6.5	346
34		13.6	15.1	1,173		-		654
1935	4,004	21.6	31.8	2,605		1935	10.9	750
36		29.3	38.7	3,425		36	11.4	759 558
37	3,941	17.9	23.5	2,192		37	7.9	816
38	4,994	23.1	32.9	3,145		38	10.8	576
39	4,406	19.4	21.1	2,175		39	8.8	576
1940	3,566	13.9	20.8	1,769		1940	7.4	543
41	3,566 3,635	14.5	20.5	1,961		41	6.3	495
42	4,219	19.5	27.6	2,320		42	8.3	570
43		36.0	36.4	3,909		43	13.3	993 538
44		20.0	20.2	2,085	T = 1 2 7	44	7.4	530
1945	4,422	22.5	27.7	2,781	•	1945	9.5	625 668
46	5,466	26.2	26.2	2,742		46	9.5	668
47	5,226	25.9	27.1	3,082		47	10.2	809
48	5,015	30.5	32.7	2,864		. 48	9.9	736
49	4,841	21.0	28.9	2,832		49	8.6	775
1950	5,760	28.5	35.7	3,730		1950	10.3	830
51		30.4	36.3	3,607		51	12.0	783
52		26.8	31.5	3,286		52	11.9	809
53		26.0	31.1	2,631		53	11.1	661
54		29.7	30.2	3,076		54	11.6	838
1955		18.5	22.0	2,222		1955	7.5	619
1956	6,523	33.1	43.0	4,246		56	14.1	1,054
		//:-				Avg.		709
Avg.	5,015			2,920		AVS.		109

Year	Natural Peak Discharge 1,000 cfs	Natural May-July Volume 1,000 A.F.	Annual Oct. Sept. Rumoff 1,000 A.F.
1904 056 078 091 1915 1916 1916 1916 1916 1916 1916 19	8.5.0.6.4.2.1.3.2.7.5.9.5.0.0.0.9.9.5.2.2.0.4.6.6.3.5.9.4.9.8.4.3.3.3.4.5.5.2.9.6.3.0.9.1.6.5.1.1.2.6.3.5.9.4.9.8.4.3.3.3.4.5.5.2.9.6.3.0.9.1.6.5.1.7.1.1.1.7.1.1.1.7.1.1.1.7.1.1.1.7.1.1.1.7.1.1.1.1.7.1	8857 59140 8811 8811 8811 8811 8811 8811 8811 8	1,302.0 780.0 899.0 1,270.0 1,124.0 1,461.0 1,461.0 1,436.0 1,49.0 1,49.0 1,238.0 1,249.0 1,249.0 1,068.0 1,07.0 944.5 968.1 1,416.0 1,331.0 866.1 797.8 9794.5 780.0 8794.0 1,149.0 1,149.0 1,049.0 1,049.0 1,149.0 1,149.0 1,049.0 1,049.0 1,14

^{1/} Reflect regulation by Jackson Lake.

54	5401 02 03 08 08 09 10	5391 93 94 96 97 5400	55	PLEV
117	100000000000000000000000000000000000000	099999999	900887654327	
3,788 3,795 4,025 4,533 4,533 4,533 7,105	1,950 2,092 2,239 2,389 2,389 2,865 3,032	729 811 899 992 1,092 1,197 1,309 1,426 1,549	162 289 515 515 538 538 538 538 538 538 538 538 538 53	STORAGE CONTENT
197 214 246 262 278 294 311	138 142 147 150 155 163 167 171	82 88 100 105 112 117 117 123 129	77 6 6 5 5 5 5 5 7 2 8 8 5 6 7 2 8 8 5 6 7 2 8 8 8 9 6 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9	DIFF. PER FT.
\$4 \$5 \$5 \$5 \$5 \$5 \$5 \$5 \$5 \$5 \$5 \$5 \$5 \$5	50 44 44 44 44 44 74 74 74 74 74 74	54 20 20 20 20 20 20 20 20 20 20 20 20 20	5421 5421 542 542 542 542 542 542 542 542 542 542	ELEV.
41,042 43,172 45,350 47,574 49,846 52,164 52,164 54,530 56,942 61,908	22,868 24,414 26,020 27,687 29,414 31,202 33,050 34,959 36,928 38,958	11,471 12,258 13,124 14,068 15,091 16,192 17,372 18,630 19,967 21,383	6,095 6,480 6,898 7,350 7,836 8,354 8,506 9,492 10,111 10,763	STORAGE
2,130 2,178 2,272 2,3318 2,412 2,566 2,460 2,566	1,546 1,606 1,667 1,727 1,727 1,9848 1,909 1,969 1,969 2,030	787 1,101 1,258 1,101 1,101 1,180 1,258 1,416	7 6 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5	DIFF. PER FT.
5491 98 99 99 99 99 99 99 99 99 99 99	5482 888 888 888 889 90	5471 72 73 77 77 78 78 80	5461 62 63 69 70	ELEV.
169,077 173,574 178,145 182,789 187,506 192,297 197,161 202,098 207,109 212,193	128,070 131,848 135,698 139,620 147,678 147,678 151,815 156,023 160,302 164,653	93,455 96,679 99,955 103,284 106,666 110,100 113,587 117,127 120,719 124,363	64,469 67,091 69,775 72,520 75,327 78,195 81,125 81,126 84,116 87,169 90,283	STORAGE
#,571 #,644 #,717 #,864 #,937 5,084 5,084	3,778 3,922 3,923 4,065 4,137 4,279 4,351	3,224 3,329 3,4329 3,543 3,540 3,540 3,707	2,622 2,684 2,745 2,807 2,930 2,930 2,991 3,114 3,114	DIFF. PER FT.
55 55 55 56 56 56 56 56 56 56 56 56 56 5	55 21 22 25 25 26 27 28 29	5511 12 14 15 16 17 18 19	5501 02 03 04 08 09	ELEV.
412,362 412,362 419,814 427,339 434,940 442,614 458,187 458,187 458,0364 474,058	343,522 348,778 355,526 362,353 369,260 376,247 383,313 390,458 397,683	273,150 279,124 285,156 291,247 297,396 303,603 309,868 316,192 322,574 329,013	217,353 222,589 227,901 233,290 238,756 244,298 249,917 255,613 261,385 267,233	STORAGE
7,376 7,4525 7,625 7,601 7,823 7,823 7,823	6,589 6,667 6,9827 7,145 7,225	5,974 6,032 6,267 6,265 6,324 6,439	5,57,55,57,57,57,57,57,57,57,57,57,57,57	DIFF. PER FT.
5571 72 73 74 76 77 78	55 66 66 66 70 66 70 66 70 66 70 66 70 70 70 70 70 70 70 70 70 70 70 70 70	55 55 55 55 55 55 55 55 55 55 55 55 55	5541 44 45 46 47 48 44 47 48 48 49 49	TEET.
758,512 768,921 779,410 789,978 800,626 811,353 822,161 833,049 844,016 855,063	658,669 668,210 678,027 687,821 697,691 707,637 717,659 727,759 727,759 748,183	566,564 575,419 584,352 593,365 602,457 611,628 620,878 630,208 639,616 649,103	482,105 490,224 498,415 506,679 515,016 523,425 531,907 540,462 549,089 557,788	STORAGE
10,409 10,568 10,568 10,648 10,727 10,888 10,888 10,961 11,047	9,541 9,817 9,794 9,870 9,946 10,022 10,100 10,174 10,250 10,329	8,855 8,933 9,013 9,092 9,171 9,250 9,487 9,487 9,566	8,119 8,119 8,191 8,264 8,409 8,627 8,627 8,776	DIFF. PER FT.
5611 12 13 14 16 17 18 19	5601 02 03 04 06 07 08	5591 93 94 96 5600	5581 82 88 88 89 90	ELEV.
1,260,630 1,275,865 1,291,207 1,306,657 1,322,215 1,337,880 1,353,653 1,369,534 1,401,618	1,115,237 1,129,178 1,143,253 1,157,461 1,171,802 1,186,276 1,200,883 1,215,624 1,230,496 1,245,503	983,906 996,356 1,008,958 1,021,712 1,034,618 1,047,676 1,060,886 1,074,248 1,074,248 1,074,762 1,101,428	866,207 877,464 888,835 900,319 911,917 923,628 935,453 947,391 959,443 971,608	STORAGE
15,235 15,342 15,558 15,665 15,988 16,096 16,096	13,941 14,075 14,208 14,341 14,474 14,607 14,741 14,872 15,007	12,450 12,602 12,754 12,958 13,058 13,210 13,362 13,514 13,666	11,257 11,371 11,598 11,711 11,825 11,938 12,052 12,1652 12,298	DIFF. PER FT.

TABLE 3
PALISADES RESERVOIR
TOTAL STORAGE CAPACITY

	67 44 44 44 44 44 44 44 44 44 44 44 44 44	6733 333 333 333 333 333 333 333 333 333	6732.0 322.1 32.2 32.4 32.5 32.6 32.6 32.9	6731.0 31.1 31.2 31.3 31.4 31.6 31.6 31.7	6730.0 30.1 30.2 30.5 30.5 30.6 30.9	ELEV.
	70,010 71,820 73,620 75,430 77,240 79,040 80,850 82,660 84,460 86,270	52,180 53,970 55,750 57,530 59,310 61,100 62,880 64,660 66,440 68,230	34,580 36,340 39,860 41,620 43,380 45,140 46,900 48,660 50,420	17,190 18,930 20,670 22,410 24,150 25,890 27,630 27,630 29,370 31,110 32,850	1,720 3,440 5,160 6,880 8,600 10,320 12,040 13,760 15,480	STORAGE CONTENT
	1810 1810 1810 1810 1810 1810 1810 1810	1790 1780 1780 1780 1780 1790 1780 1780 1780 1780	1760 1760 1760 1760 1760 1760 1760 1760	1740 1740 1740 1740 1740 1740 1740 1740	1720 1720 1720 1720 1720 1720 1720 1720	STOR
	6739. 39.2 39.2 39.5 39.6 39.8 39.8	6738.1 388.1 388.2 388.5 388.5 388.6 388.9	6737 37 37 37 37 37 37 37 37 37 37 37	6736. 36.2 36.2 36.5 46.5 36.6 36.8	673 333 335 355 555 987 655 100 100 100 100 100 100 100 100 100 1	BLEV.
	163,030 164,980 166,930 168,880 170,830 172,780 174,730 174,730 176,680 178,630 180,580	143,860 147,690 147,690 149,610 151,450 153,450 155,360 155,280 157,280 161,120	124,980 126,870 128,760 130,650 134,420 134,420 136,310 136,310 140,080 141,970	106,390 108,250 110,110 111,970 113,830 115,690 117,550 119,410 121,270 123,130	88,070 89,910 91,740 93,570 95,400 97,230 97,230 100,900 102,730 104,560	STORAGE
	1950 1950 1950 1950 1950 1950 1950	1920 1910 1920 1920 1920 1920 1920 1920	1890 1890 1890 1890 1890 1890	1860 1860 1860 1860 1860 1860 1860	1840 1830 1830 1830 1830 1840 1830 1830 1830	STOR
	67##.0 ##.1 ##.2 ##.5 ##.5 ##.6 ##.8	67#3.0 #3.1 #3.2 #3.5 #3.5 #3.6 #3.7 #3.8	67+2.0 +2.1 +2.2 +2.3 +2.5 +2.6 +2.6 +2.7 +2.8	67#1.0 #1.1 #1.2 #1.3 #1.4 #1.5 #1.6 #1.6 #1.7	6740.0 40.1 40.2 40.3 40.4 40.5 40.6 40.6 40.8	ELEV.
	263,500 267,690 269,790 271,880 271,980 273,980 276,070 278,170 280,260	242,830 244,900 246,960 249,030 251,100 253,170 255,230 257,300 259,370 261,440	222, 430 224, 470 228, 550 230, 590 232, 630 234, 670 234, 710 238, 750 240, 790	202,330 204,340 206,350 208,370 210,370 212,380 214,390 214,390 216,400 218,410 220,420	182,520 184,510 186,490 188,470 190,450 192,430 194,410 196,390 198,370 200,350	STORAGE
	2100 2090 2100 2090 2100 2100 2100 2100	2070 2070 2070 2070 2070 2070 2070 2070	2040 2040 2040 2040 2040 2040 2040	2010 2010 2010 2010 2010 2010 2010 2010	1980 1980 1980 1980 1980 1980 1980	STOR
	67 ⁴ 9.0 49.1 49.2 49.3 49.5 49.6 49.8	6748.0 48.1 48.2 48.3 48.5 48.6 48.6 48.6 48.9	6747.0 47.1 47.2 47.3 47.5 47.6 47.6 47.7	67+6.1 +66.1 +66.2 +66.3 +66.3 +66.3	674 445 445 455.2 455.3 455.3 5.8	ELEV.
	370,750 372,960 375,180 377,400 377,610 381,820 381,820 386,260 388,470 390,680	348,820 351,010 353,210 355,400 357,590 359,780 361,980 364,170 368,560	327,120 329,290 331,460 333,630 335,800 337,970 340,140 342,310 344,480 346,650	305,660 307,810 309,950 312,100 314,240 316,390 318,540 322,680 322,830 322,830	284,450 286,570 288,690 290,810 292,930 295,050 297,180 299,300 301,420 303,540	STORAGE
	2210 2220 2220 2210 2210 22210 22220 22220 22210 22210	21 90 2200 21 90 21 90 21 90 22 90 22 90 21 90 21 90 21 90 21 90 21 90	2170 2170 2170 2170 2170 2170 2170 2170	2150 2140 2150 2150 2150 2150 2150 2150 2150 215	2120 2120 2120 2120 2120 2120 2120 2120	STOR
		6753. 533. 533. 533. 53. 53. 53. 6	6752.0 52.1 52.2 52.5 52.5 52.6 52.6 52.8	6751.0 51.2 51.2 51.3 51.4 51.5 51.6 51.6 51.7 51.8	6750.0 50.1 50.2 50.4 50.5 50.6 50.6 50.8	ELEV.
	483,470 485,780 488,090 490,390 492,700 495,010 497,320 497,320 499,630 501,930 504,240	#60,550 #62,850 #65,140 #67,430 #69,720 #72,010 #74,300 #74,300 #78,890 #78,890	437,810 440,090 444,640 444,910 446,910 449,180 453,730 456,010 458,280	415,260 417,520 419,770 422,030 424,280 426,540 426,540 428,790 431,050 433,300 435,560	392,900 395,140 397,370 399,610 401,840 404,080 406,320 408,550 410,790 413,020	STORAGE
	2310 2310 2300 2310 2310 2310 2310 2310	2290 2290 2290 2290 2290 2290 2290 2290	2270 2270 2270 2270 2270 2270 2270 2270	2 2 2 2 3 5 6 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	2240 2230 2240 2230 2240 2240 2240 2230 2240 2230 223	STOR
	6759. 599.1 599.2 599.5 599.5 599.7	6755 558 5588.10 5588.21 5588.55 56.87	6757.0 57.1 57.2 57.3 57.6 57.6 57.6 57.7	6756.0 556.1 556.1 556.5 556.6 56.6	6755 555.0 555.2 555.2 555.2 555.2 555.2 555.2	ELEV.
	600,470 602,860 605,250 607,640 610,020 612,410 614,800 617,190 619,580	576,750 579,120 581,490 583,870 586,240 588,610 590,980 593,350 595,730	553,190 557,900 560,260 562,610 564,970 567,330 569,680 572,040 571,390	529,790 532,130 534,470 536,810 539,150 541,490 541,490 548,510 548,510	506,550 508,870 511,200 513,520 515,850 518,170 520,490 522,820 522,820 527,470	STORAGE
	23990 23990 23990 23990 23990 23990 23990	2370 2370 2380 2370 2370 2370 2370 2370 2380 2370 2370	2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2	2340 2340 2340 2340 2340 2340 2340 2340	2330 2330 2330 2330 2330 2330 2330 2330	STOR
	67.67 64.75	67.63.10 63.5.4.5 63.63.5.4.5 63.63.5.4.5 63.63.63	6762.0 62.1 62.2 62.3 62.4 62.5 62.6 62.6 62.8	6761.0 61.2 61.3 61.4 61.5 61.6 61.6 61.7	6760.0 60.1 60.2 60.5 60.6 60.7	ELEV.
	721,560 724,030 726,500 728,980 731,450 733,920 736,400 736,400 741,340 741,340	697,000 699,460 701,920 704,370 706,830 709,280 711,740 714,190 716,650 719,100	672,620 675,060 677,500 679,940 682,370 684,810 687,250 689,690 692,130	648,400 650,830 655,670 658,090 660,510 662,930 667,780 670,200	624, 360 626, 760 629, 160 631, 570 633, 980 636, 380 638, 780 641, 190 643, 600	STORAGE
	2470 2470 2470 2470 2470 2470 2470 2470	2460 2460 2460 2460 2460 2460 2460 2460	2440 2440 2440 2440 2440 2440 2440 2440	2420 2420 2420 2420 2420 2420 2420 2420	2400 2410 2410 2410 2410 2410 2410 2410	STOR
	6769.0 69.1 69.5 69.6 69.6 69.6	6768.0 68.1 68.3 68.5 68.6 68.6 68.7 68.8	6767.0 67.1 67.2 67.3 67.6 67.6 67.6	6766.0 66.1 66.2 66.5 66.6 66.9	6765.0 655.2 655.2 65.3 65.6 65.8	ELEV.
1	847,000 849,530 852,100 854,660 857,220 857,220 862,350 864,910 867,480 872,600	821,520 824,070 826,610 829,160 831,700 834,250 836,790 839,340 841,880 841,420	796,260 798,790 801,320 803,840 806,370 808,900 811,420 811,420 813,950 816,470 819,000	771,180 773,690 776,200 778,710 781,220 783,720 786,230 788,740 791,250 793,760	746,280 748,780 751,260 753,760 756,240 758,740 761,220 762,720 766,200 768,700	
	222222 25570 25570 25570 25570	25550 25550 25550 25550 25550 25550	2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2	2510 2510 2510 2510 2510 2510 2510 2510	2480 2500 2500 2500 2500 2500 2500 2500 25	STOR

TABLE 4
JACKSON LAKE RESERVOIR
USABLE STORAGE CAPACITY

TABLE 5
REPRESENTATIVE SNOW COURSE DATA

Snow	Map	Eleva- tion		—y	l ct	~	15th	— B 0	Reco	February		e Water March		March		15th	Inches	Inches 5th April 1st	Inches Sth April 1st April	Inches 5th April 1st April 15	5th April 1st April 15th May 1	5th April 1st April 15th May 1st	Sth April 1st April 15th May 1st
Course	No.	m.s.l		Years	E.	Years W	Ħ	Years	E.	Years	W.E.	Years		W.E.	W.E. Years	ম	E. Years W	E. Years W.E.	.E. Years W.E. Years W	.E. Years W.E. Years W.E.	.E. Years W.E. Years W.E. Years W	.E. Years W.E. Years W.E. Years W.E.	.E. Years W.E. Years W.E. Years W
Afton R.S.	<u> </u>	6,2	200	19	2.2	1	8	21	3.8	1	1	21		4.7	4.7 -	.7	.7 -	.7	.7 21 2	.7 - 21 2.1	.7 21 2.1 1	.7 21 2.1 1 0.0	.7 21 2.1 1 0.0 4 0.
Aster Creek	2	7,700	00	5	14.4	31	14.5	6	25.0	32	22.1	6		32.1	32.1 32	i	.1 32 27.	.1 32 27.2	.1 32 27.2 8 39.	.1 32 27.2 8 39.6	.1 32 27.2 8 39.6 32 29	.1 32 27.2 8 39.6 32 29.8	.1 32 27.2 8 39.6 32 29.8 1 45.
Blackrock	G.	8,6	600	1	ā	l l	1	33	12.6	1	1	7		20.6	0	6	-6	.6	.6 20 22	.6 - 20 22.9	.6 20 22.9 -	.6 20 22.9	.6 20 22.9 3 25.
CCC Camp	+	7,500	00	19	4.5	8	1	21	7.7	6	1	21		10.1	10.1 -	0.1	0.1	0.1	0.1 21 11.	0.1 21 11.9	0.1 21 11.9 1 15.	0.1 21 11.9 1 15.0	0.1 21 11.9 1 15.0 7 4.
d	5	7,500	00	2	7.4	ı	1	Н	11.2	ŝ	ı	3		14.1	14.1		ā	8	18	18 17.5	18 17.5 -	18 17.5	18 17.5 1 10.
Coulter Creek	6	7,6	600	5	9.1	30	11.0	6	17.1	32	16.7	6		22.2	22.2 32	12	.2 32 20	.2 32 20.3	.2 32 20.3 8 26.	.2 32 20.3 8 26.4	.2 32 20.3 8 26.4 30 21.	.2 32 20.3 8 26.4 30 21.0	.2 32 20.3 8 26.4 30 21.0 -
Deadman Ranch	7	6,534	34	10	4.1	1	1	12	6.5	ı	80	20		9.9	9.9 -	9	.9	9 -	.9 19 1	.9 19 10.7	.9 19 10.7 -	.9 19 10.7	.9 19 10.7 5 1.
East Rim Divide	00	7,950	50	6	3.8		1	N	7.1	1	1	17		10.2		N	.2 1 12	.2 1 12.4	.2 1 12.4 21 12.	.2 1 12.4 21 12.1	.2 1 12.4 21 12.1 1 13.	.2 1 12.4 21 12.1 1 13.1	.2 1 12.4 21 12.1 1 13.1 10 10.
Four-Mile Meadows	9	7,7	770	1	1	1	1	33	8.3	4	1	7	1	12.3	12.3 -	ů.	-3	-3	.3 21 13	.3 21 13.4	.3 21 13.4 -	.3 21 13.4	.3 21 13.4
Glade Creek	10	7,200	00	6	9.5	31	11.6	6	16.7	32	17.4	6		21.7	21.7 32	.7 3	.7 32 21	.7 32 21.4	.7 32 21.4 8 26.	.7 32 21.4 8 26.0	.7 32 21.4 8 26.0 32 22.	.7 32 21.4 8 26.0 32 22.8	.7 32 21.4 8 26.0 32 22.8 1 32.
Grover Park Divide	 .de 11	7,500	00	19	4.4	1	1	20	7.5	ı	1	21		10.1	10.1	i	1	1	- 21 11.	.1 - 21 11.6	.1 21 11.6 1 14	.1 21 11.6 1 14.7	.1 21 11.6 1 14.7 7 4.
Huckleberry Divide	de 12	7,	300	0,	8.4	31	9.7	6	14.8	32	14.9	0		19.0	9.	9.0	9.0 32 18.	9.0 32 18.0	9.0 32 18.0 7 22.	9.0 32 18.0 7 22.8	9.0 32 18.0 7 22.8 32 18.	9.0 32 18.0 7 22.8 32 18.8	9.0 32 18.0 7 22.8 32 18.8 1
Lewis Lake Divide	le 13	7,900	000	6	19.8	31	20.7	6	33.1	32	30.7	0		42.9		9	.9 32 37.	.9 32 37.9	.9 32 37.9 8 51.	.9 32 37.9 8 51.3 3	.9 32 37.9 8 51.3 32 42.	.9 32 37.9 8 51.3 32 42.0	.9 32 37.9 8 51.3 32 42.0 5
Togwotee Pass	14	9,600	00	1	ı	1		33	18.9	1	ı	7		27.6		0	.6	1	.6 - 21 29.	.6 - 21 29.6	.6 21 29.6 -	.6 21 29.6	.6 21 29.6 7 35
Turpin Meadows	15	6,	930	ı	t	ı	ı	33	6.9	1	ı	7		10.6	0	0.6	0.6	0.6	0.6 - 21 10.	0.6 21 10.9	0.6 21 10.9 -	0.6 21 10.9	0.6 21 10.9
Yellowjacket	16	7,675	575	+	1.9	1	1	9	4.3	1	5.2	15		5.8		ω	.8 1 5	.8 1 5.7	.8 1 5.7 20 6	.8 1 5.7 20 6.7	.8 1 5.7 20 6.7 1 5.	.8 1 5.7 20 6.7 1 5.6	.8 1 5.7 20 6.7 1 5.6 7 0.

TABLE 6
RATING TABLE

SNAKE RIVER NEAR HEISE, IDAHO

Γ	GAGE	DIS-		GAGE	DIS-		GAGE	DIS-		GAGE	DIS-	-
	HGHT	CHARGE	DIFF	HGHT	CHARGE	DIFF		CHARGE	DIFF	1	CHARGE	DIFF
-	FEET	Cfs	Cfs	FEET	Cfs	Cfs	FEET	Cfs	Cfs	FEET	Cfs	Cfs
	1.00			5.00	11,040	360	9.00	30,270	570			
	.10			.10	11,400	360	.10	30,840	570			
l	.20			.20	11,760 12,130	770	.20	31,410 31,980	570			
١	.40	1,830		.40	12,500	370	.40	32,550	570			
ĺ	.50	1,940	110	.50	12,880	380	.50	33,120	570			
l	.60	2,060	120 130	.60	13,270		.60	33,690	570			
	.70	2,190	150	.70	13,670	11.00	.70	34,260	570 570			
l	.80	2,340	160	.80	14,070 14,480	117.0	.80	34,830 35,400	570			
	.90	2,500	180	.90	14,400	420	.90	77,400	600			
	2.00	2,680		6.00	14,900		10.00	36,000	(
l	.10	2,880	200	.10	15,330	450	.10	36,600	600 600			
	.20	3,100	220	.20	15,770	10100	.20	37,200	600			
	.30	3,320 3,550	230	.30 .40	16,210 16,660	11.50	.30	37,800 38,400	600			
	.50	3,780	230	.50	17,110	450	.50	39,000	600			
	.60	4,020	240	.60	17,560	450	.60	39,600	600			
	.70	4,260	240 250	.70	18,020	100	.70	40,200	600			
	.80	4,510	260	.80	18,490	1100	.80	40,800	600			
	.90	4,770	270	.90	18,970	490	.90	41,400 42,000	600			
							11.00	42,000				
	3.00	5,040	270	7.00	19,460	500	y 11					
	.10	5,310 5,580	270	.10 .20	19,960 20,470	E10						
	.30	5,850	270	.30	20,470	510						
	.40	6,130	280	.40	21,490	210						
	.50	6,410	280 280	.50	22,000							
	.60	6,690	280	.60	22,520	F00						
	.70	6,970 7,260	290	.70 .80	23,040	FOO						
	.90	7,550	290 290	.90	23,560 24,100	540						
	.,,	1,000	290	.,0	21,200	550						
0.117	4.00	7,840		8.00	24,650							
	.10	8,130	290	.10	25,210	500						
	.20	8,420	290 290	.20	25,770	500						
	.30	8,710	300	.30	26,330	560 560				=	p.s.	
	.40	9,010 9,310	300	.40 .50	26,890 27,450	F(A					e:	
	.60	9,510	320	.60	28,010	560						
	.70	9,970	340	.70	28,570	560						
	.70 .80	10,320	350 360	.80	29,130	500						
	.90	10,680	360	.90	29,700	570 570						
						710						

Data from USGS table dated 12-28-54

TABLE 7

RATING TABLE

SNAKE RIVER AT MORAN, WYOMING

,			-						
	GAGE	DIS-		GAGE	DIS-		GAGE	DIS-	
	HGHT	CHARGE	DIFF	HGHT	CHARGE	DIFF	HGHT	CHARGE	DIFF
1	FEET	Cfs	Cfs	FEET	Cfs	Cfs	FEET	Cfs	Cfs
1	1.00	3	5.3	5.00	2,110	100	9.00	8,050	180
1	.10	8.3	9.2	.10	2,210	100	.10	8,230	180
1	.20	17.5 28	10.5	.20	2,310	110	.20	8,410	190
	.30	40	12	.30	2,420	110	.30	8,600	190
	.50	54	14	.50	2,530 2,640	110	.40	8,790 8,980	190
	.60	70	16	.60	2,760	120	.60	9,170	190
1	.70	90	20	.70	2,880	120	.70	9,360	190
	.80	114	24	.80	3,000	120	.80	9,550	190
1	.90	140	26	.90	3,120	120	.90	9,740	190
			28			130		771	190
	2.00	168	30	6.00	3,250	130	10.00	9,930	200
-	.10	198	32	.10	3,380	130 130	.10	10,130	200 200
	.20	230	35	.20	3,510	130	.20	10,330	200
1	.30	265	38	.30	3,640	140	.30	10,530	200
	.40	303 345	42	.40	3,780	140	.40	10,730	200
	.50 .60	390	45	.50	3,920 4,070	150	.50	10,930	200
	.70	435	45	.70	4,220	150	.70	11,130 11,330	200
	.80	480	45	.80	4,370	150	.80	11,530	200
1	.90	530	50	.90	4,520	150	.90	11,730	200
		,,,,	50	- , ,	.,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,	150	11.00	11,930	200
			-						
-	3.00	580		7.00	4,670	7.50	,		
	.10	635	55 55	.10	4,820	150 160			
	.20	690	55	.20	4,980	160			
	.30	745	55	.30	5,140	160			
	.40	800	60	.40	5,300	160			
	.50	860 930	70	.50	5,460	160			
	.70	1,000	70	.60	5,620 5,790	170	1		
	.80	1,070	70	.70	5,960	170			
	.90	1,140	70	.90	6,130	170			
	•) •	2,2.0	70	.,0	0,170	170			
	4.00	1,210	90	8.00	6,300	7.50			
	.10	1,290	80	.10	6,470	170			
	.20	1,370	80	.20	6,640	170			
	.30	1,460	90	.30	6,810	170			
	.40	1,550	90	.40	6,980	170 170			
	.50	1,640	90	.50	7,150	120			
	.60	1,730	90	.60	7,330	180			
	.70	1,820	90	.70	7,510	180			
	.90	2,010	100	.80	7,690	180			
	• 30	2,010	100	.90	1,010	180			
		from HC	og teb	_		11.7			

Data from USGS table dated 12-31-43

TABLE 8

DISCHARGE RATING TABLE

SNAKE RIVER NEAR SHELLEY, IDAHO

1								
GAGE HEIGHT Feet	DISCHARGE c.f.s.	DIFF.	GAGE HEIGHT Feet	DISCHARGE	DIFF.	GAGE HEIGHT Feet	DISCHARGE	DIFF. c.f.s.
3.00 .10 .20 .30 .40 .50 .60 .70 .80	470 500 540 580 620 670 720 770 820 870	30 40 40 50 50 50 50 60	7.00 .10 .20 .30 .40 .50 .60 .70 .80	6,370 6,700 7,030 7,360 7,700 8,040 8,380 8,730 9,080 9,430	330 330 330 340 340 350 350 350 360	11.00 .10 .20 .30 .40 .50 .60 .70 .80	21,370 21,800 22,240 22,680 23,120 23,560 24,000 24,450 24,900 25,350	430 440 440 440 440 440 450 450 450
4.00 .10 .20 .30 .40 .50 .60 .70 .80	930 990 1,060 1,140 1,230 1,320 1,410 1,500 1,600 1,700	60 70 80 90 90 90 100 100	8.00 .10 .20 .30 .40 .50 .60 .70 .80	9,790 10,150 10,510 10,870 11,230 11,600 11,970 12,340 12,710 13,080	360 360 360 360 370 370 370 370 370	12.00 .10 .20 .30 .40 .50 .60 .70 .80	25,800 26,250 26,700 27,160 27,620 28,080 28,540 29,000 29,460 29,920	450 450 460 460 460 460 460 460 460
5.00 .10 .20 .30 .40 .50 .60 .70 .80	1,810 1,930 2,060 2,210 2,370 2,540 2,720 2,910 3,110 3,320	120 130 150 160 170 180 190 200 210	9.00 .10 .20 .30 .40 .50 .60 .70 .80	13,450 13,820 14,190 14,560 14,940 15,320 15,710 16,100 16,500 16,900	370 370 370 380 380 390 390 400 400			
6.00 .10 .20 .30 .40 .50 .60 .70	3,540 3,770 4,010 4,260 4,520 4,790 5,090 5,410 5,730 6,050	230 240 250 260 270 300 320 320 320 320	10.00 .10 .20 .40 .50 .60 .70	17,300 17,700 18,100 18,500 18,900 19,300 19,710 20,120 20,530 20,950	400 400 400 400 410 410 410 420 420			

Data from USGS table dated 12-27-54

TABLE 9

DISCHARGE RATING TABLE

HENRYS FORK NEAR REXBURG, IDAHO

GAGE HEIGHT Feet	DISCHARGE c.f.s.	DIFF.	GAGE HEIGHT Feet	DISCHARGE c.f.s.	DIFF.	GAGE HEIGHT Feet	DISCHARGE c.f.s.	DIFF.
.00 .10 .20 .30 .40 .50 .60 .70 .80			4.00 .10 .20 .30 .40 .50 .60 .70 .80	1,340 1,410 1,480 1,550 1,620 1,690 1,760 1,840 1,920 2,000	70 70 70 70 70 70 80 80 80	7.00 .10 .20 .30 .40 .50 .60 .70 .80	3,850 3,950 4,050 4,150 4,260 4,370 4,490 4,610 4,740 4,870	100 100 100 110 110 120 120 130 130
.00 .10 .20 .30 .40 .50 .60 .70 .80	570 620 670	50 50 50	5.00 .10 .20 .30 .40 .50 .60 .70 .80	2,080 2,160 2,240 2,320 2,400 2,490 2,570 2,660 2,750 2,830	80 80 80 90 80 90 90	8,00 .10 .20 .30 .40 .50 .60 .70 .80	5,000 5,140 5,280 5,420 5,560 5,700 5,850 6,010 6,180 6,350	140 140 140 140 140 150 160 170 170
3.00 .10 .20 .30 .40 .50 .60 .70 .80	720 775 830 890 950 1,010 1,070 1,130 1,200 1,270	55 55 60 60 60 60 70 70	6.00 .10 .20 .30 .40 .50 .60 .70 .80	2,920 3,010 3,190 3,280 3,370 3,460 3,550 3,650 3,750	90 90 90 90 90 90 100 100	9.00 .10 .20 .30 .40 .50 .60 .70 .80	6,520 6,700 6,880 7,060 7,240 7,420 7,600 7,780 7,960	180 180 180 180 180 180 180

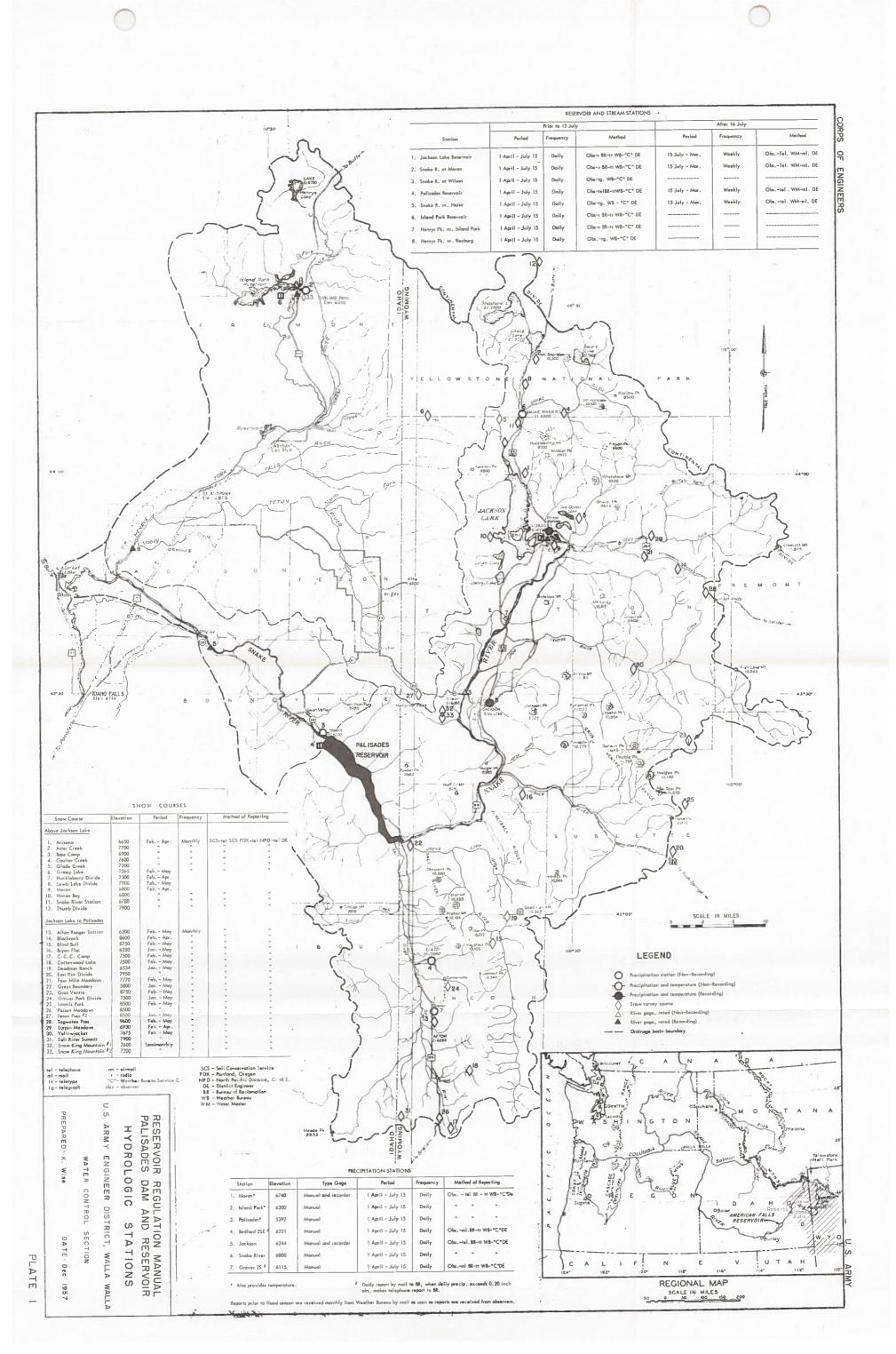
Data from USGS table dated 12-29-50

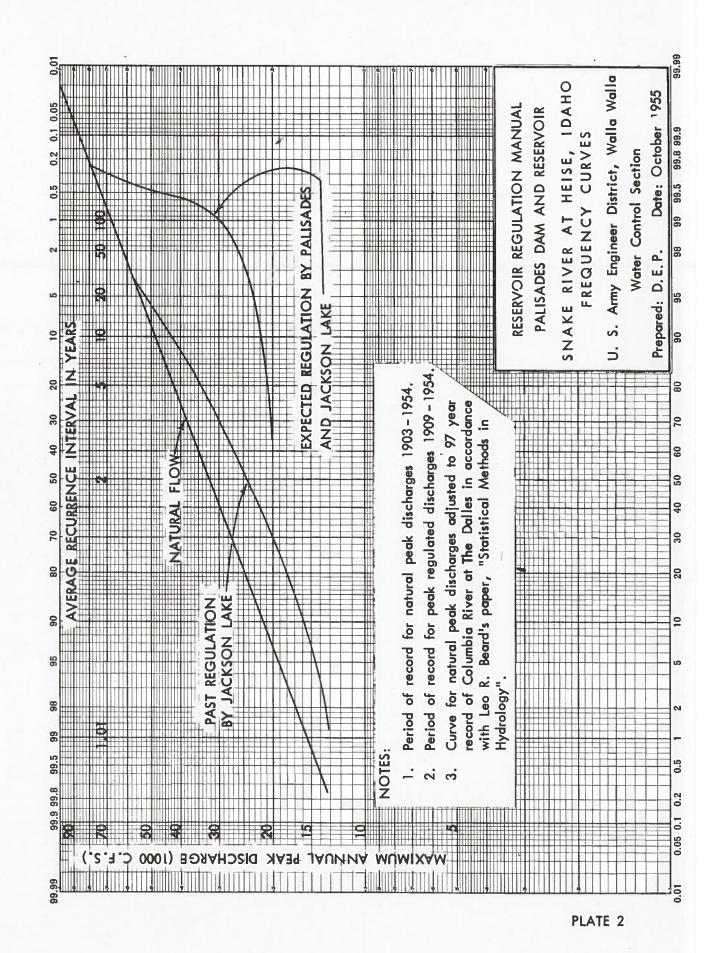
SNAKE RIVER AT MORAN, WYOMING Natural Flow In 1,000 Acre-feet

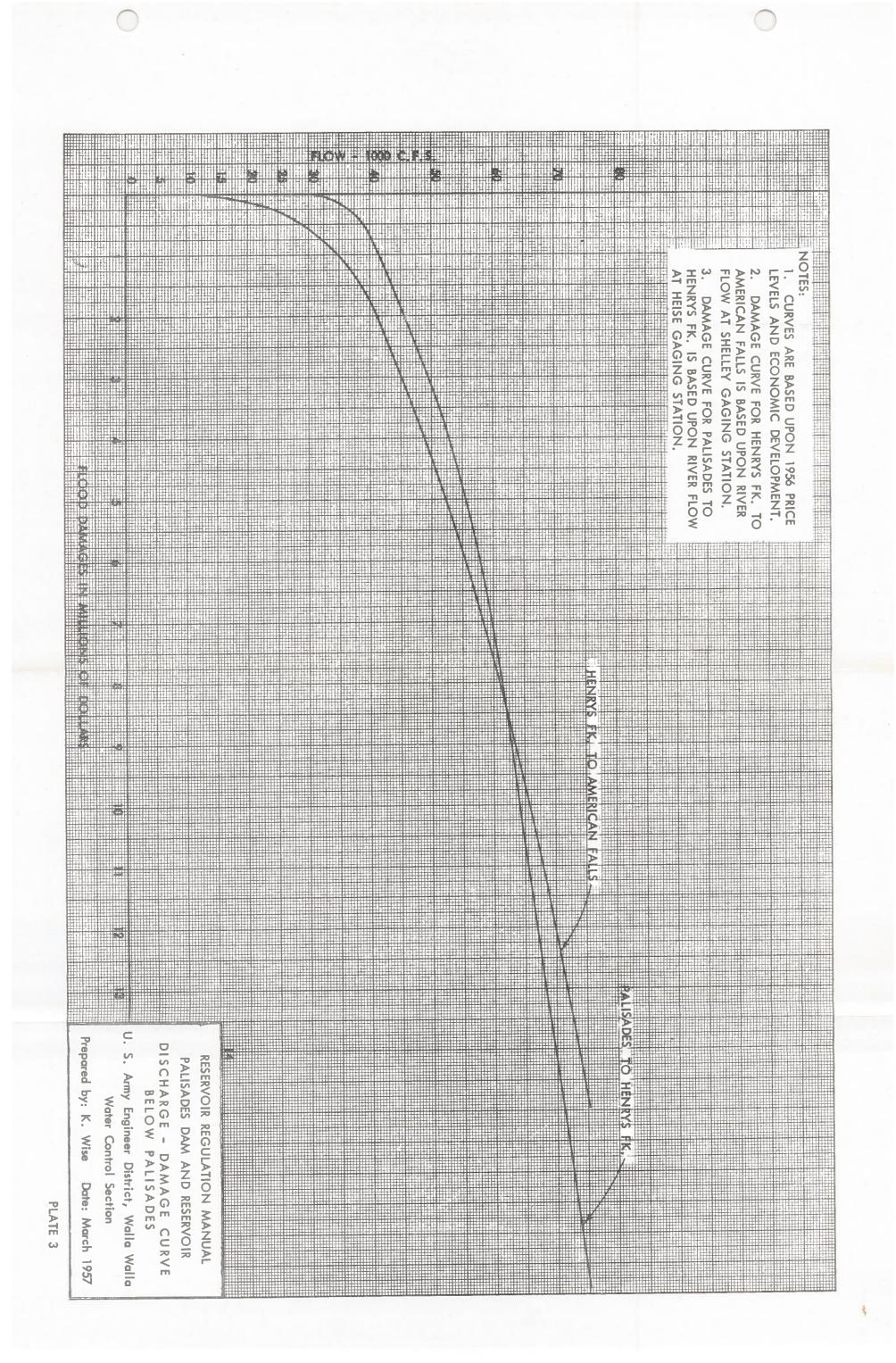
-			2000									
911	30.8	25.1			37.1	31.0	38.4	206.4	539.5	249.5	67.0	36.4
912	41.2	43.1	22.2	29.4	35.9	32.0	36.1	133.6	6.625	205.8	103.6	51.3
913	58.2	39.8	39.2	45.8	33.9	35.7	62.0	308.9	457.7	203.2	107.6	44.0
914	48.1	45.9	32.7	42.9	39.3	32.7	57.2	298.9	330.3	238.0	43.1	57.3
915	60,1	49.1	31.4	24.3	17.0	27.4	7.96	139.2	181.8	82.7	30.8	30.8
.916	23.9	29.0	28.1	37.4	33.6	37.9	47.0	174.9	421.5	279.0	74.0	36.0
917	35.2	27.3	39.5	27.5	31.4	33.8	30.0	141.3	435.9	303.0	92.2	40.8
918	25.7	24.0	9.47	33.3	30.0	28.4	35.2	166.2	601.2	150.7	73.3	35.6
919	46.2	29.1	22.3	23.7	28.7	31.9	42.5	234.5	139.7	39.3	26.6	20.7
920	26.2	29.8	30.0	28.0	23.1	28.6	30.0	173.3	360.0	162,1	67.8	39.2
921	6.04	32.0	33.3	33.1	23.6	24.5	35.3	285.9	342.3	129.0	54.9	33.2
922	25.7	33.6	34.0	29.2	26.8	25.1	24.8	179.4	393.6	142.0	59.3	34.1
923	20.3	21.5	29.2	31.8	22.6	27.9	31.7	197.0	321.9	159.7	50.1	30.9
924	30.1	24.3	27.4	27.8	23.2	19.5	30.4	216.2	141.8	67.3	20.0	20.0
925	42.0	30.3	28.0	31.8	31.8	26.5	74.2	357.2	369.1	202.8	83.2	47.7
926	45.3	31.6	26.5	23.1	26.0	22.6	78.6	244.5	148.1	67.4	37.5	21.2
927	28.6	35.2	35.2	35.4	36.7	23.0	37.4	189.8	597.5	258.2	82.7	55.3
1928	40.5	61.0	49.5	39.9	26.4	32.5	48.6	478.9	293.1	171.7	58.5	32.5
929	31.4	23.9	33.6	29.5	27.3	27.2	35.0	149.6	314.4	115.7	47.6	31.3
1930	22.7	14.4	27.5	18.5	26.4	22.6	67.3	185.8	207.4	98.8	64.1	31,5
931	43.2	24.1	20.0	20.2	16.5	23.1	37.7	148.7	148.4	4.7.4	29.5	17.2
1932	21.7	19.6	24.8	26.4	26.7	29.6	35.4	228.3	358.5	135.9	61.5	24.8
1933	20.0	20.1	22.1	31.3	27.5	19.3	25.3	118.5	390.4	112.1	53.2	33.0
934	21.0	19.4	19.9	28.4	20.8	28.7	111.5	208.7	86.2	48.9	20.7	38.4
935	27.8	28.2	27.6	30.3	22.9	26.1	45.2	167.9	353.7	135.0	51.3	19.6
1936	21.9	23.4	19.6	40.1	38.0	27.7	0.99	382.5	283.5	91.3	51.6	23.3
937	17.5	13.0	21.4	24.4	27.3	21.2	28.5	230.2	232.1	100.0	107.0	19.1
938	24.5	22.6	32.1	29.2	26.6	36.1	50.9	223.2	438.2	157.8	64.1	41.3
939	31.2	27.9	30.5	28.5	28.3	26.1	66.1	307.6	191.4	106.8	51.5	26.4
940	23.0	14.0	19.0	26.7	29.4	27.6	48.7	264.5	205.4	73.3	38.4	24.5
941	26.1	24.5	22.9	26.9	22.1	18.4	31.7	225.4	186.0	9.48	62.8	47.2
942	40.4	31.7	40.4	27.9	24.8	20.4	59.2	160.0	278.8	133.3	55.1	23.0
943	16.5	35.2	35.9	43.9	29.5	32.7	98.7	240.3	481.4	275.7	87.0	42.1
576	33.6	29.8	23.1	19.8	22.7	25.6	29.0	168.6	242.6	126.0	9.99	22.2
945	19.3	25.5	19.9	23.9	28.4	23.0	23.6	171.4	287.0	175.2	66.5	32.6
946	29.1	31.4	34.9	33.0	35.8	35.6	105.2	271.3	268.0	121.2	50.6	36.5
244	27.4	29.1	33.0	30.4	21.6	28.3	33.6	337.8	323.8	147.7	66.1	43.3
1948	28.8	29.6	26.8	29.6	26.4	26.1	41.3	247.7	368.0	119.9	52.3	29.4
676	25.2	29.9	33.3	29.3	28.3	30.6	67.7	338.6	314.5	121.6	55.7	32.9
950	32.0	27.0	23.9	35.5	34.2	33.9	40.5	160.6	442.4	217.3	70.2	9.04
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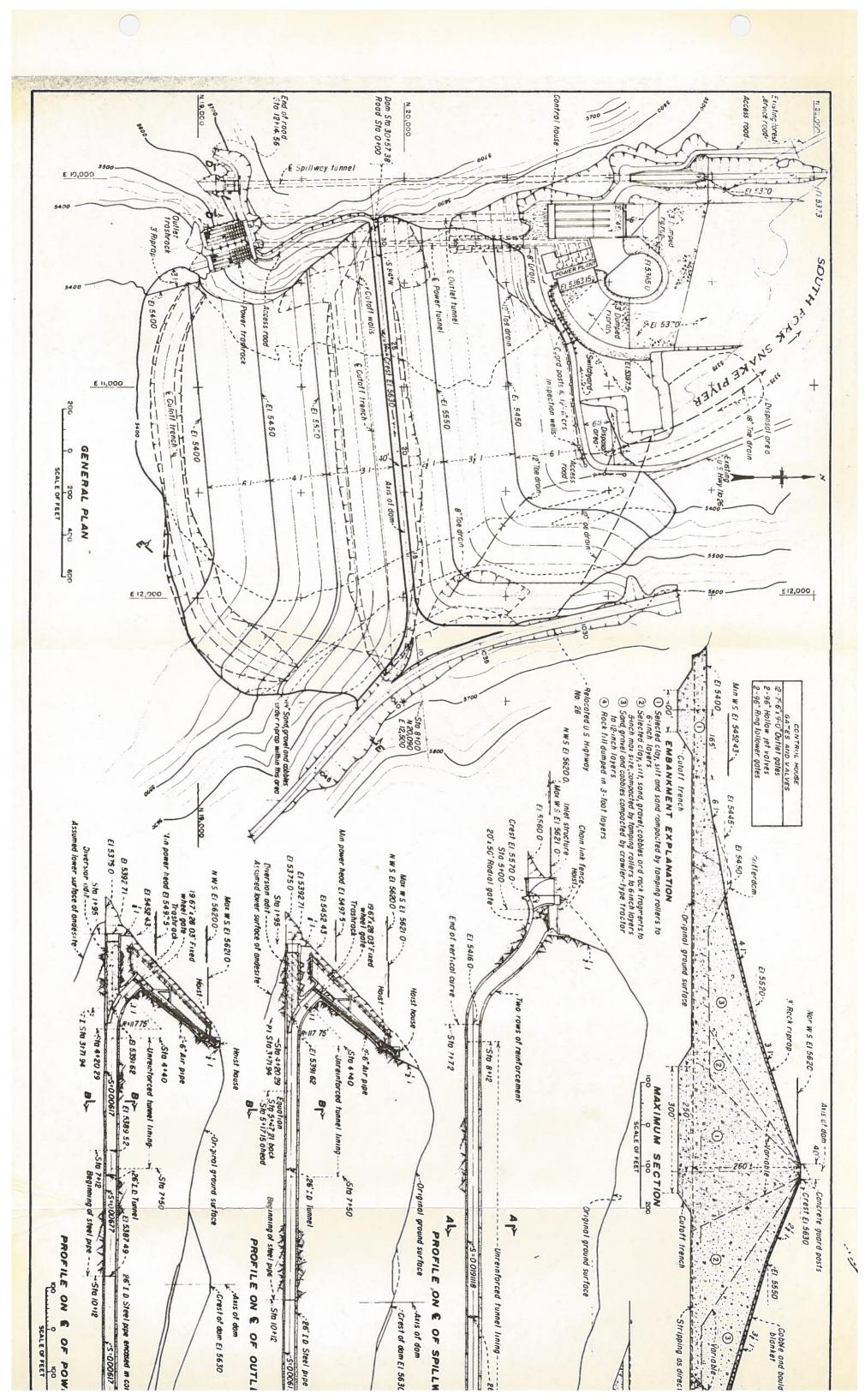
SNAKE RIVER AT HEISE, WYOMING Natural Flow In 1,000 Acre-feet

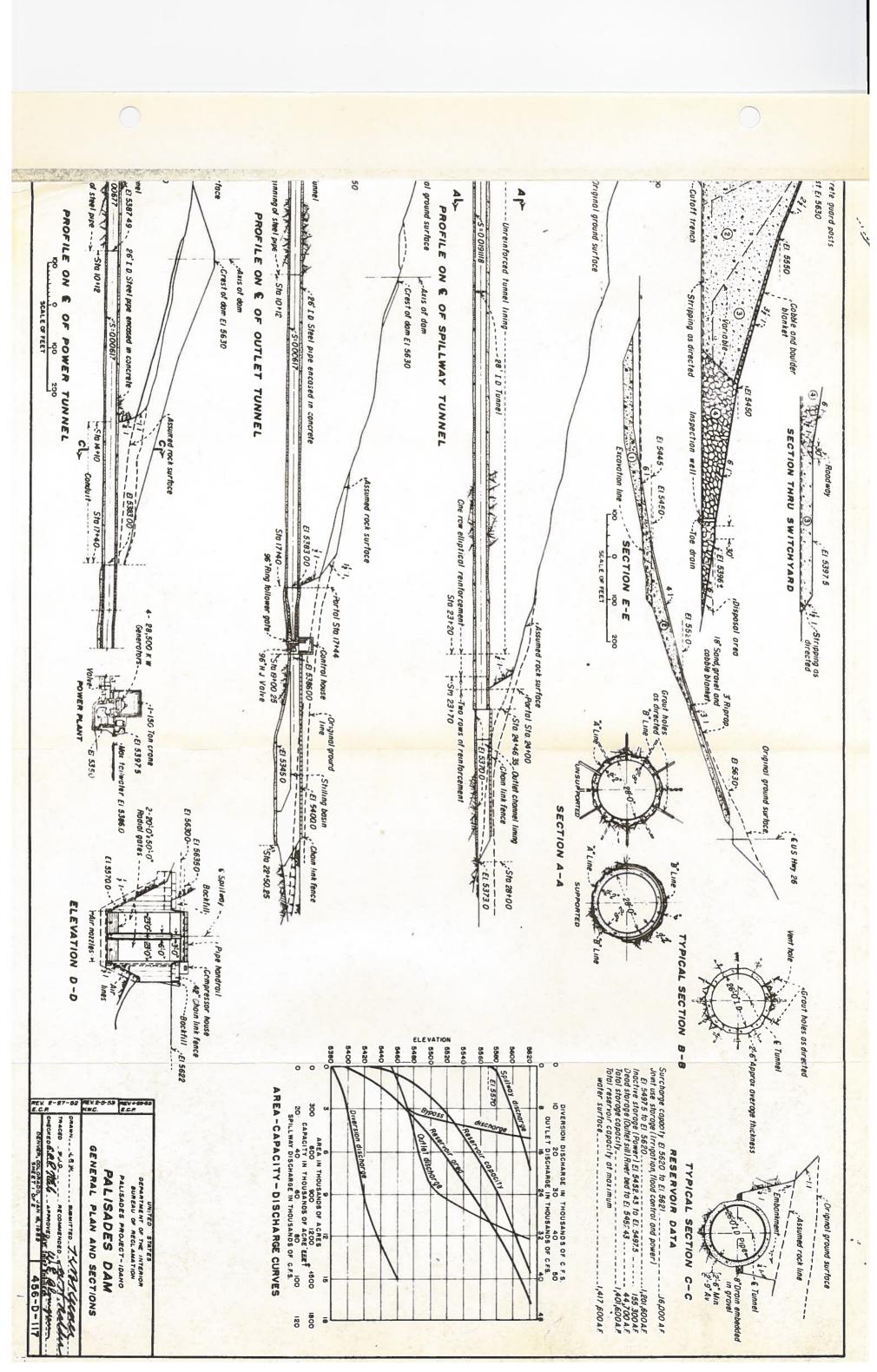
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Sept.	2.50,5	300.9	336.3	298.0	312.4	233.9	289.0	339.9	283.6	179.3	274.6	284.7	284.1	244.9	180.4	332.2	195.9	344.3	257.5	267.3	247.6	160.2	236.8	213.0	127.6	198.4	241.9	189.7	253.8	217.5	184.9	256.4	204.8	289.2	200.8	303.0	262.5	271.5	223.2	230.3	311.3	251 6	, , ,
Aug.	3511	795.0	439.6	434.67	352.15	262.8 6	455.0	480.2	392.3	196.9	355.8 +	364.9	379.3	357.9	198.0	422.780	253.5	428.7	361.5	294.6	354.14	150.8	337.5	268.2	150.7	274.2	315.4	219.8	328.0	274.6	191.1	305.6	254.8	460.3	257.4	391.7	308.3	404.7	281.0	281.2	422.76	7 928	
July	4.5	2	43.8	247	94.1	58.1	0	0	7	7	LIT	0	0	0	9	8	4	2	7	7	8	4	_	1	4	36	3	0	0	8	5	2	.	_	10	6.50	7	_	- +	10	071.1%	6 6 6	
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May			00	9.79	52,7	4		_			77					410		_			6.3					10					27/2					6.9					976.6	1005.0	
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Mar.	170.3	203.8	181.5	193.7	187.8	176.611	240.5	184.0	259.5	252.4	156.5	238.5	186.8	198.8	174.1	188.7	213.8	163.3	219.6	172.5	178.277	165.6	154.1	157.2	176.0	137.1	143.6	146.9	170.8	194.9	171.9	154.6	147.5	166.1	163.6	155.6	205.8	198.2	159.0	176.5	188.1 2	177.7	
Feb.	7	186.7	169.5	186.26	168.3	159.49	177.1	167.0	216.5	210.3	143.2	200.9	164.9	165.9	183.0	165.2 4	161.6	170.1	180.6	171.7	149.9	143.3	133.2	150.6	130.8	118.4 \$	146.4	135.4	139.4	152.8	150.4	127.7	140.4	152.3	163.9	150.4%	162.6	156.4	156.2	152.3	167.5	160.7	
Jan.			176.8	216.8 1	200.74	192.20	169.9	171.7	252.1	219.2	156.0 €	229.4	182.1	202.9	167.6	177.4	169.5	195.8	243.2	179.3	156.5 %	153.7	143.9	184.2	157.3	137.65	158.6	142.8	159.3	181.1	154.23	147.3	157.8	183.9	173.3	156.9	179.2	168.1	177.9	159.7	178.1	177.3	
Dec.			178.1	215.3	204.8	204.3	172.9	201.8	300.5	235.8	146.2	235.6	235.9	194.3	176.2	156.3 %	200.9	198.6	255.8	187.6	184.45	176.4	182.3	175.0	253.7	139.1	146.4	168.8	179.4	192.9	153.7	149.4	199.6	186.2	197.2	167.14	205.3	212.2	187.2	185.8	181.4	192.9	
Nov.		201.6	226.6	245.14	249.2	243.9	178.0	213.0	277.9	259.6	180.0	239.3	228.5	193.3	194.4	184.7	225.9	206.4	298.4	207.5	177.43	202.3	198.9	193.6	169.0	146.6	166.3	173.3	172.4	206.3	157.6	163.3	195.1	193.0	228.4	187.1	223.6	212.4	207.6	197.6	208.65	205.8	
Oct.	90		247.73		285.6 %	320.8	219.4	272.0	287.2	315.7	201.0	261.2	230.5	209.9	231.6	232.8	274.5	213.8	297.2	249.5	221.6	288.5	171.2	214.1	186.1	157.6	180.8	206.3	191.3	236.6		181.6	234.5			190.2		253.4	233.9		- 1	234.7	
Year		1911	1912	1913 300	1914	1915	1916	1917	1918	1919	1920	1921	1922	1923	1924	1925	1926	1927	1928	1929	1930	1931	1932	1933	1934	1935	1936	1937	1938	1939	1940	1941	1942	1943	1944	1945	1946	1947	1948	1949	1950	Ave.	

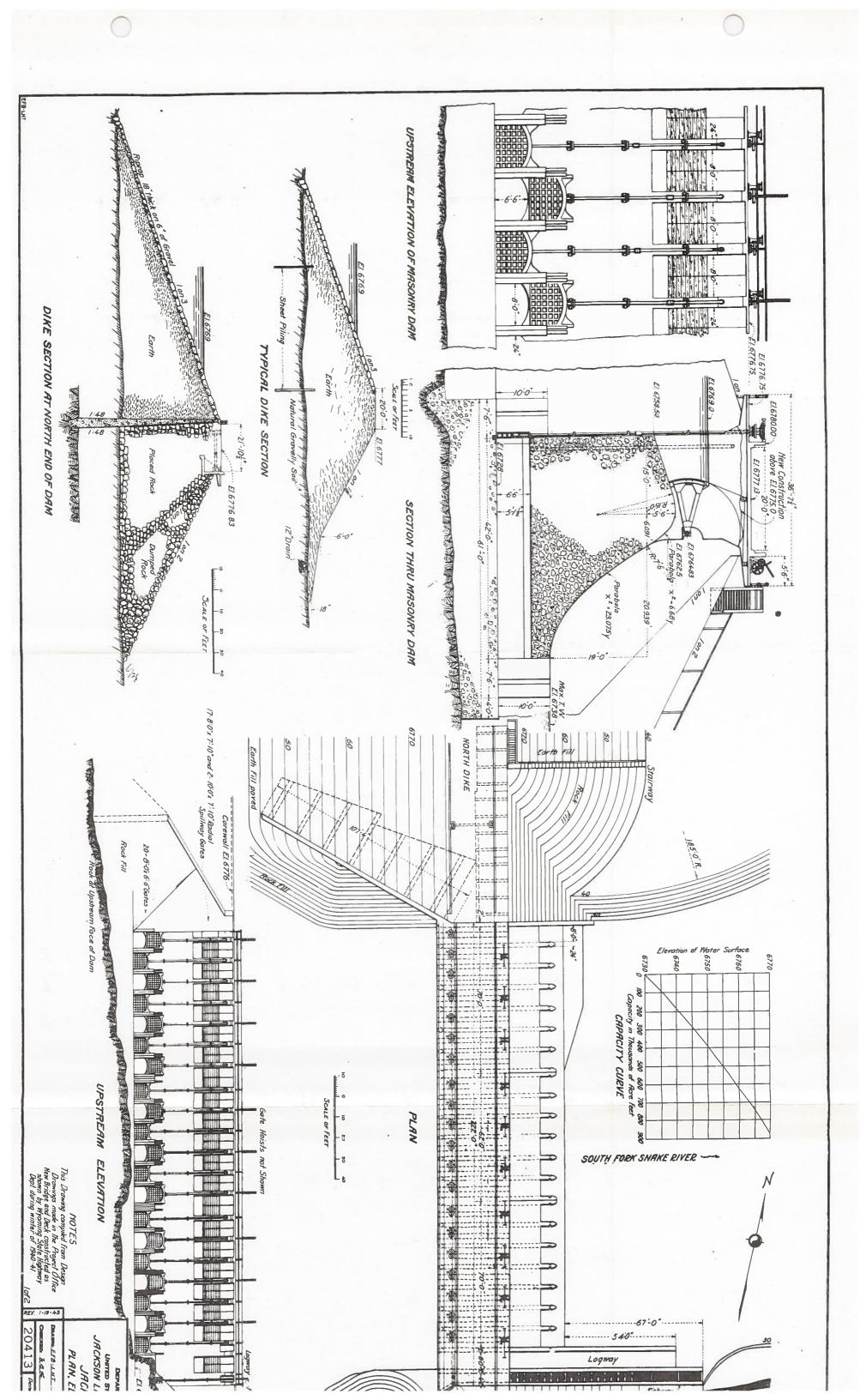












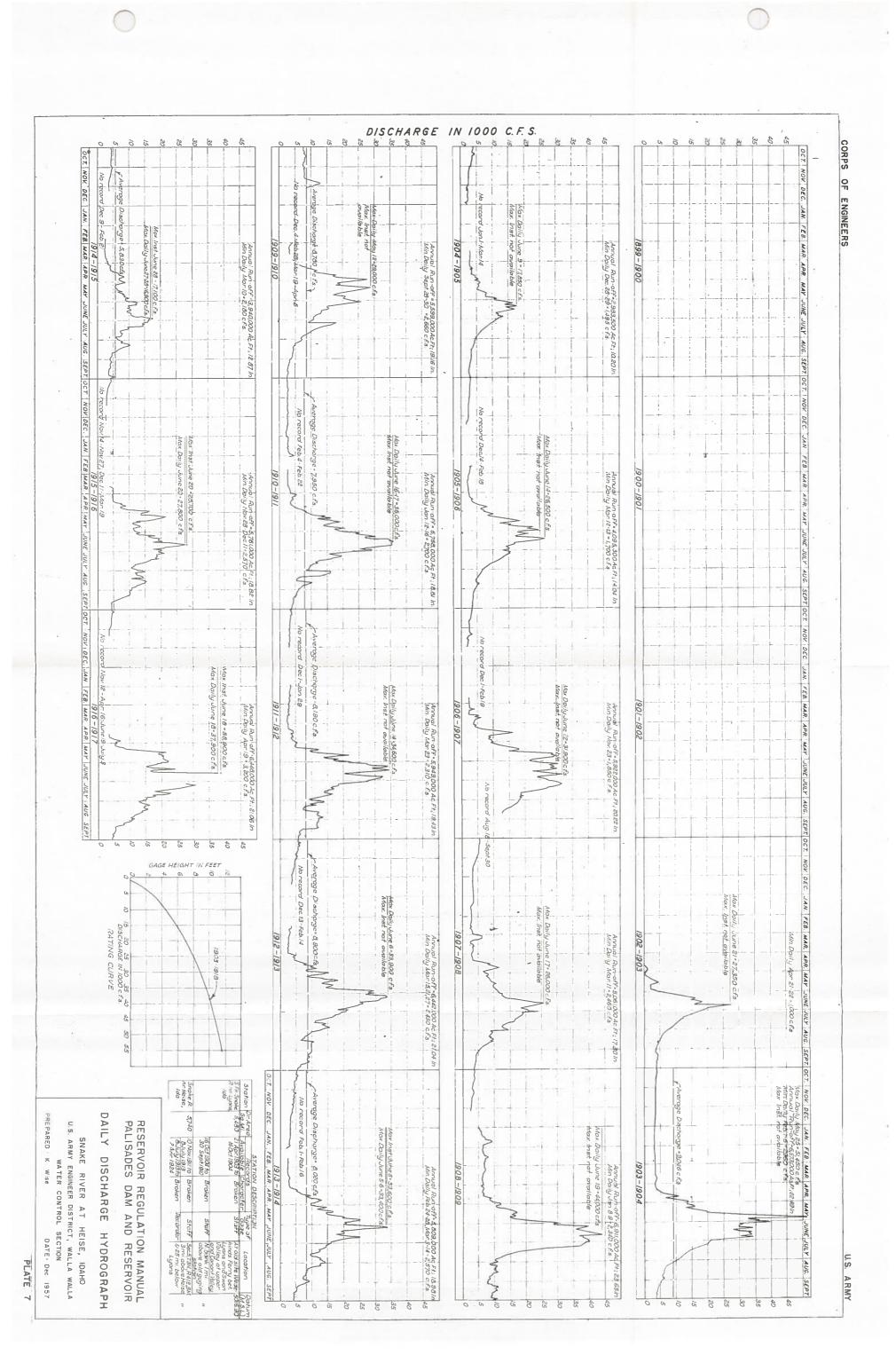
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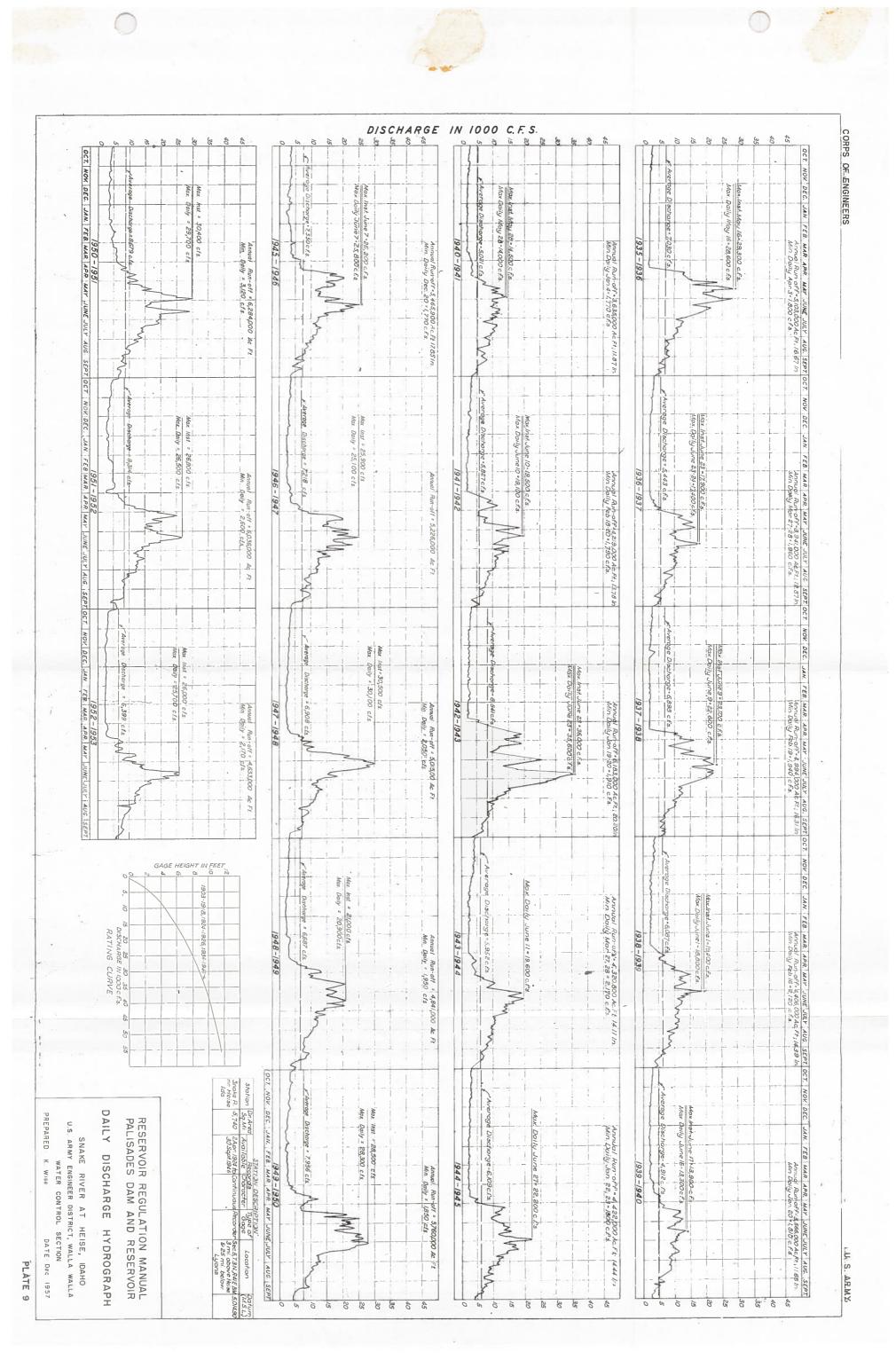
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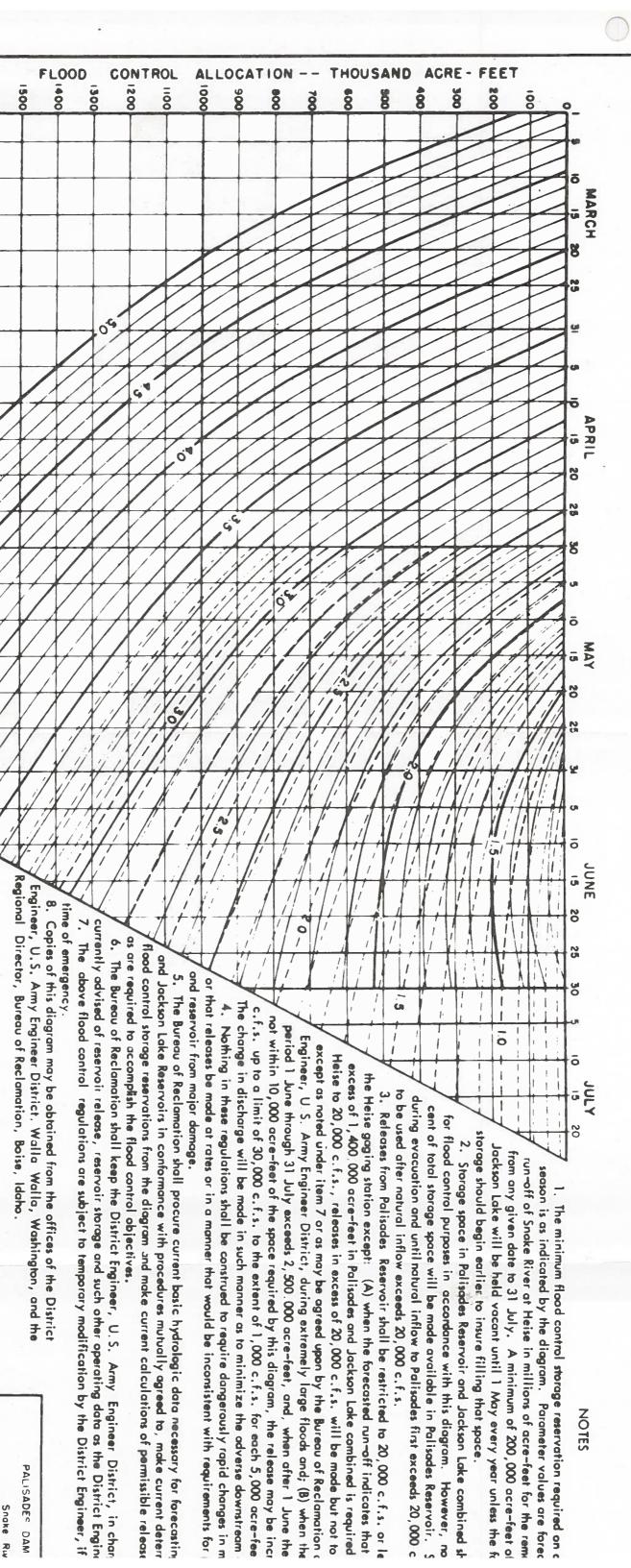
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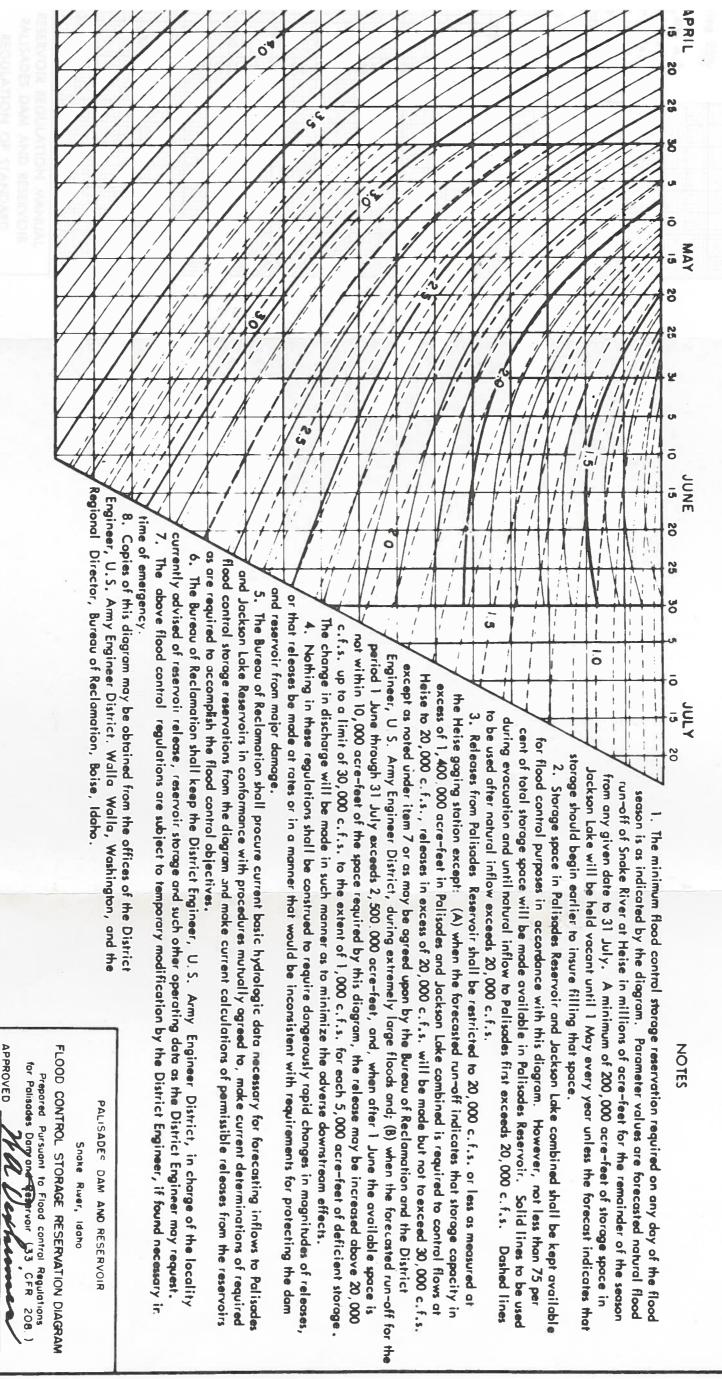
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FLOOD CONTROL STORAG

Prepared Pursuant to



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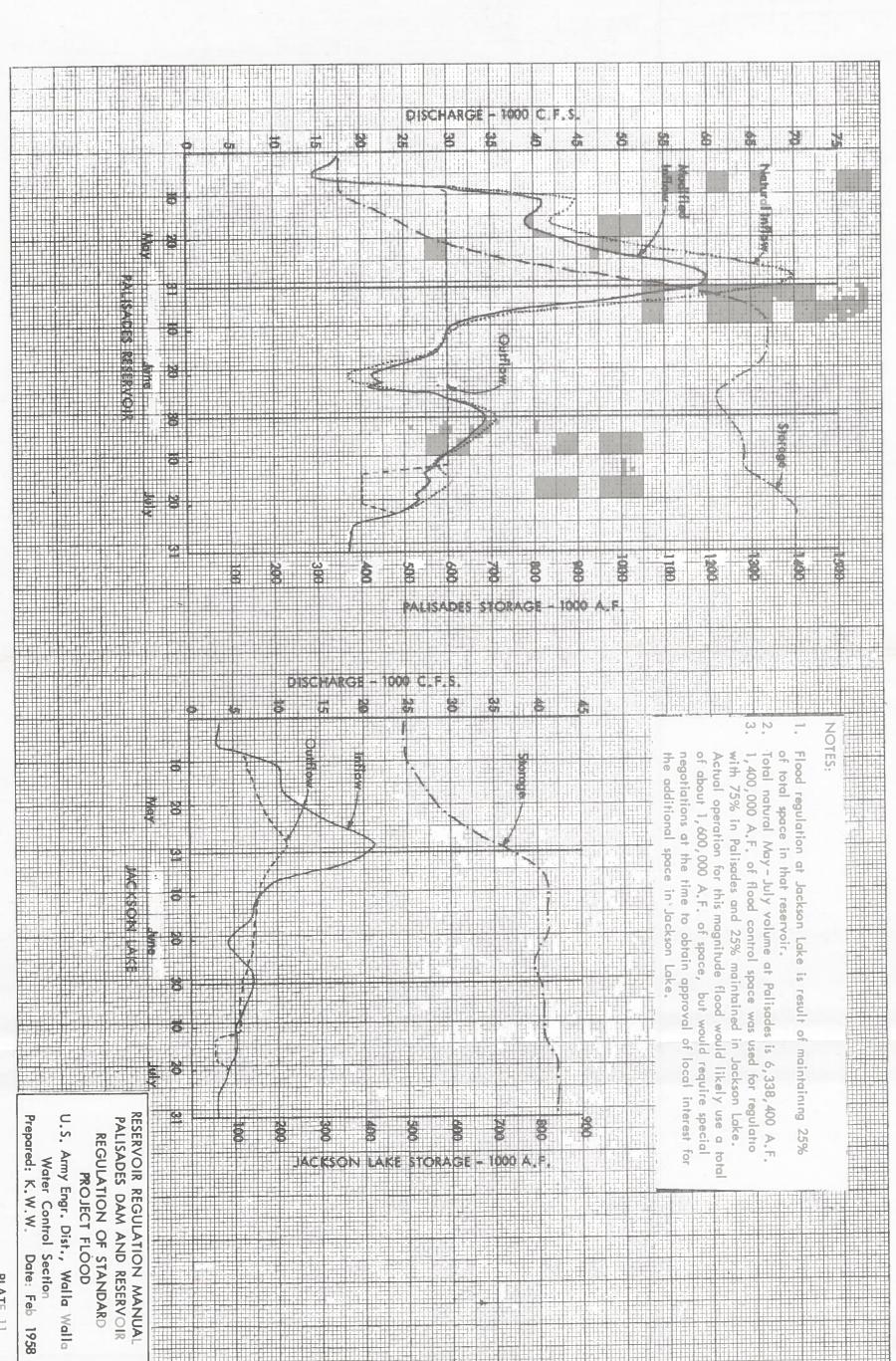
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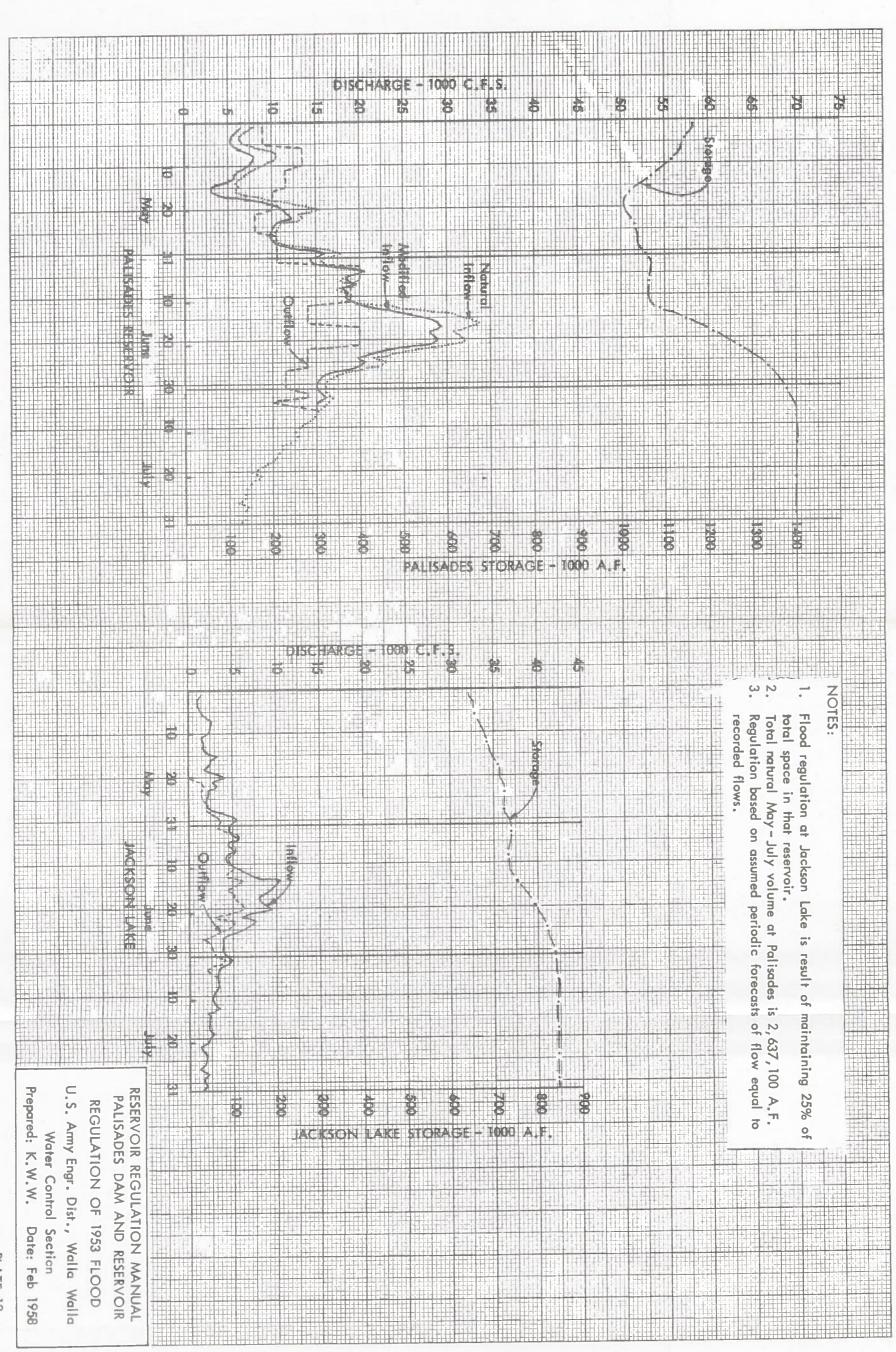
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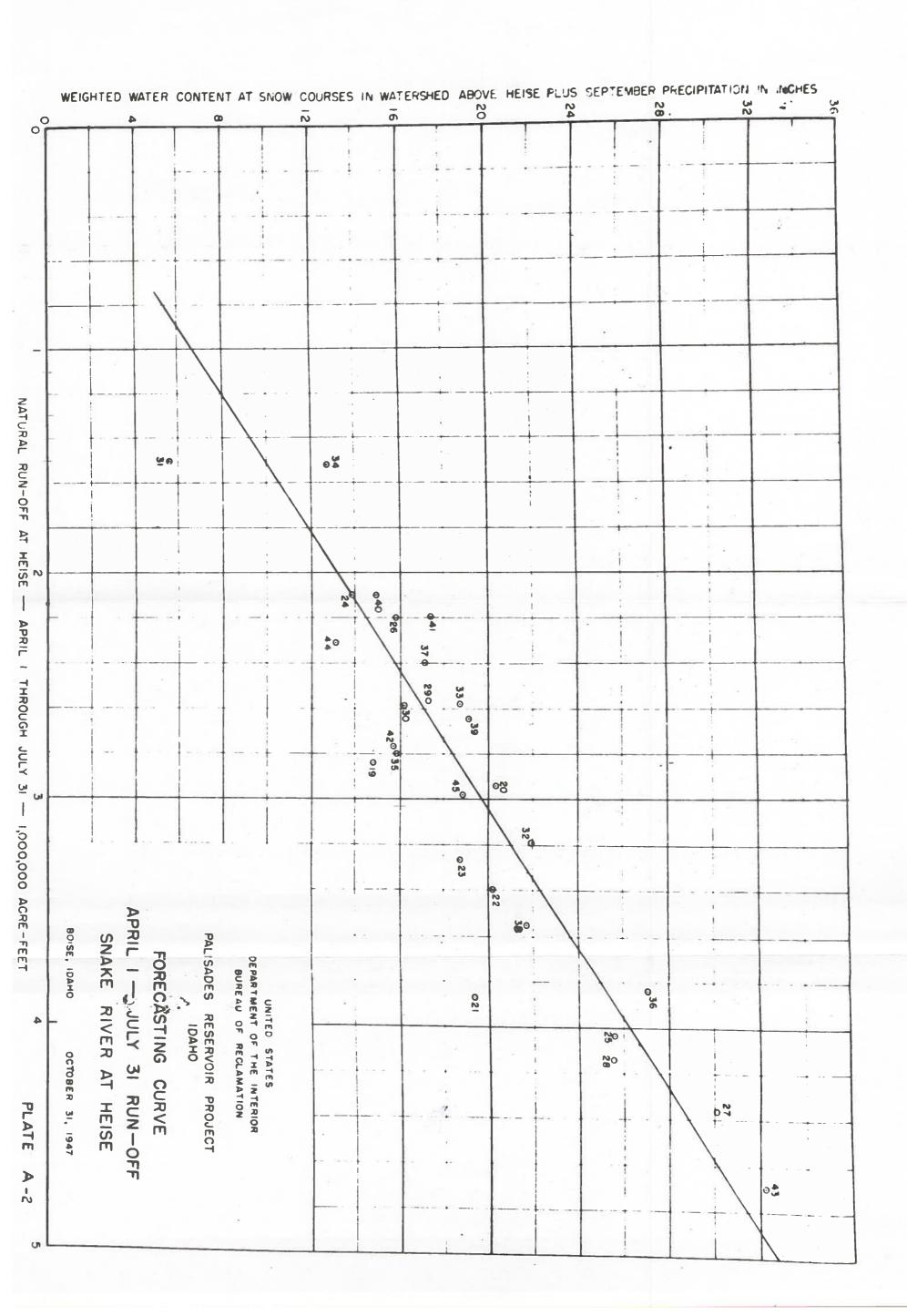
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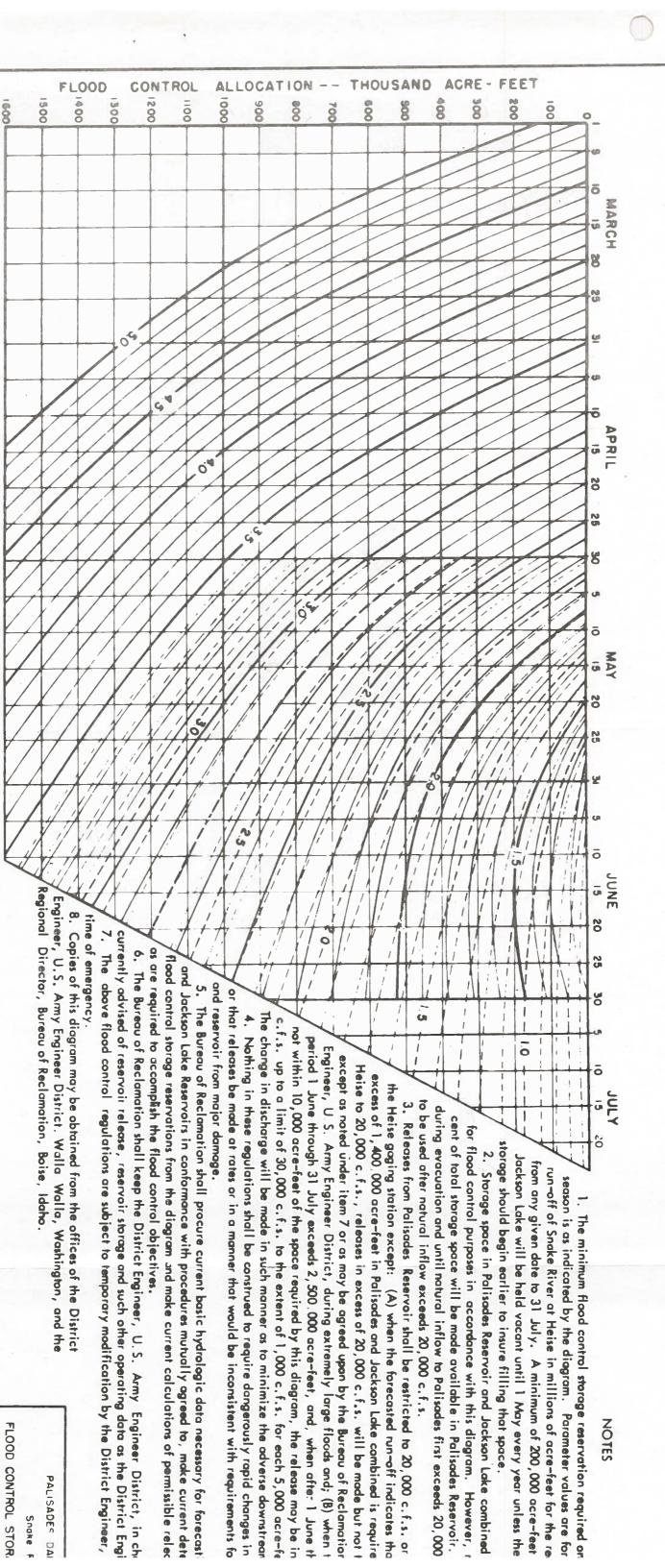
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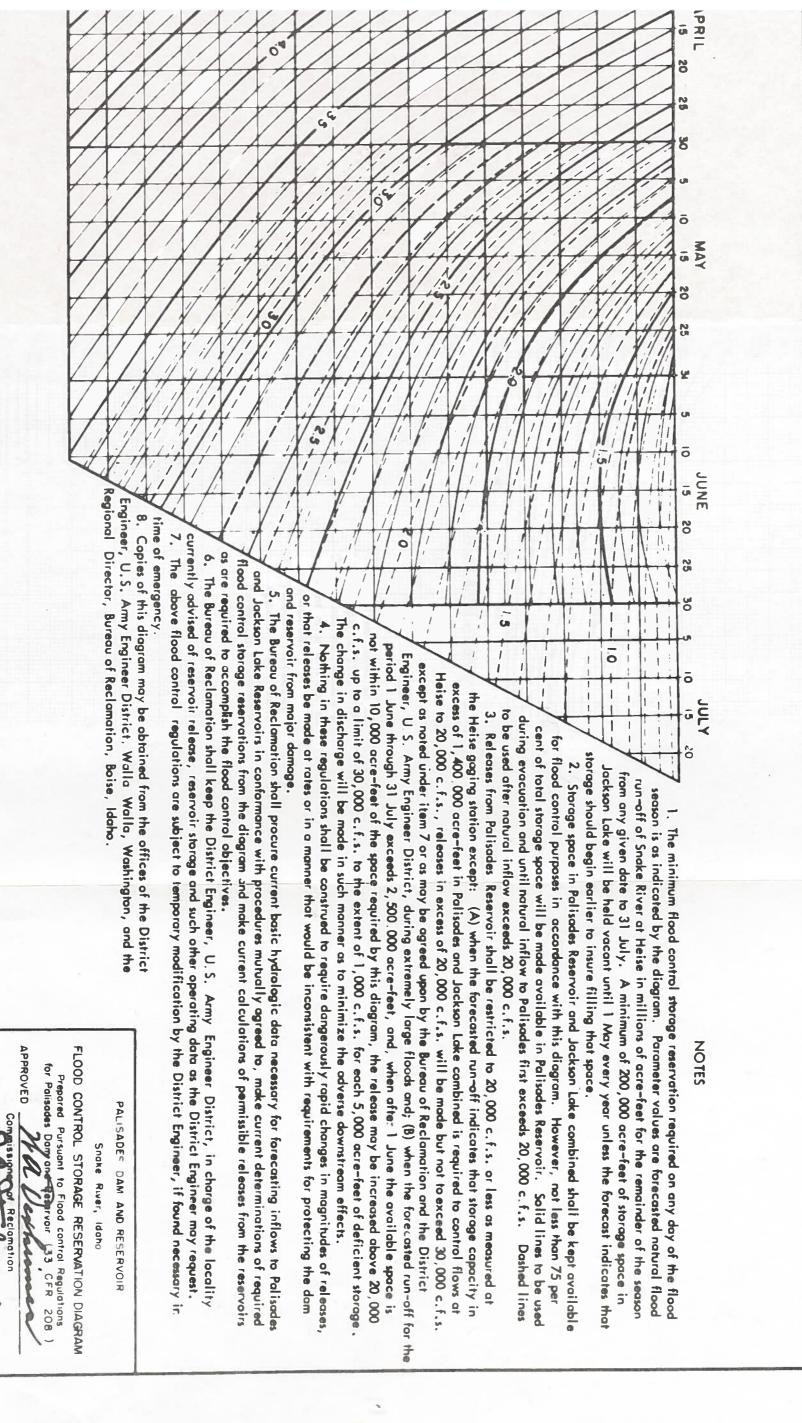
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Prepared Pursuant to



General, Chief of Engineers

Johnson

958 File No SN-902-1/1

Effective Date May 12, 1

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APPENDIX A

ORIGINAL OPERATING PLAN - 1948

Palisades Project

The Bureau of Reclamation plans to construct and operate Palisades Reservoir for the optimum multiple-purpose use of the entire storage of 1,400,000 acre-feet. To attain this objective, the storage below elevation 5,497 feet mean sea level, approximating 200,000 acre-feet, will be reserved for dead storage and allocated exclusively to the production of hydroelectric power and the maintenance of a permanent pool for the preservation and propagation of fish and wildlife. The remainder of the storage capacity in the amount of 1,200,000 acre-feet will be operated in the joint interests of irrigation and flood control governed by the best available runoff forecasts.

The Bureau of Reclamation will forecast from time to time during the period from 1 February to 31 July of each year, on the basis of precipitation, temperature, snow survey and runoff data, the volume of runoff that may be expected in the drainage area tributary to the Snake River above Heise, Idaho. To the extent that such services can be arranged for by cooperative agreements, the Bureau of Reclamation will make the forecasts hereunder after consultation with the Reclamation Engineer of the State of Idaho or his authorized representative, and the Chief of Engineers or his authorized representative. To facilitate the forecasting of runoff the Bureau of Reclamation will expand the existing hydrologic network and will establish and operate continuously a system for the efficient assembling and analyzing of the basic data. Until such time as a better method of forecasting be devised, the forecasts will be based upon estimates of area-elevation weighted snow water content as determined from periodic snow surveys on or about 1 February, 1 March, 1 April, and 1 May, and upon precipitation for September of the preceding year. A sample curve of the correlation between weighted snow water content on 1 April of a given year plus precipitation of the preceding September and the resultant runoff from 1 April to 31 July, inclusive, of the year in question, is shown on Plate II.

To the end of accomplishing the optimum multiple-use of the reservoir, the Bureau of Reclamation, beginning with the first year the reservoir is put into operation, will operate the reservoir on the basis of the forecasted runoff as nearly as practicable in accordance with the following plan:

1. For the purpose of rules and regulations to be prescribed by the Secretary of the Army under Section 7 of the Flood Control Act of 1944 (58 Stat. 887, 890) the storage space allocated to flood control is defined as follows:

It is the reservoir space which, using the governing forecast of flood runoff for the year, according to the curves shown on Plate I is required to the end of controlling the forecasted flood volume from the time in that year that reservoir inflow first exceeds 20,000 second-feet through the succeeding 31 July releases from the reservoir during that period such that the flow at the Heise gage will not exceed 20,000 second-feet, insofar as this control can be accomplished with a reservoir capacity not exceeding 1,200,000 acrefeet. The governing forecast of flood volume for each year is the forecast made as of the day when reservoir inflow in that year first exceeds 20,000 second-feet.

The parameters shown on Plate I, empirically derived from floods of record, are enveloping curves of the storage requirements for various volumes of total forecast runoff from any given date to 31 July. The reservoir capacity required to control the flood to a discharge of 20,000 second-feet (or less) below the dam is indicated by the ordinate of the parameter corresponding to the forecasted runoff on the date when the inflow to the reservoir exceeds 20,000 second-feet.

- 2. During the period of each year from the date of the first forecast about 1 February to the date of making the governing forecast for that year (approximately the middle of May) herein designated as the evacuation period, the reservoir will be operated in such a manner that the required reservoir level as determined by the parameters on Plate I at the time inflow to the reservoir exceeds 20,000 second-feet can be attained with minimum practicable rates and fluctuations of discharge. The rate of discharge during the evacuation period would be determined as follows: The reservoir level required on or about 15 May (the date on which inflows normally may be expected to exceed 20,000 second-feet) would be estimated by use of the parameters on Plate I and a 15 May forecast would be derived by deducting probable minimum inflows for the intervening period from the date of periodic forecasts beginning on 1 February. The reservoir levels thus estimated would comprise tentative allocations of flood control space at which to aim the evacuation procedure. The rate of discharge then would be selected as that required to release the probable maximum inflow for the period between date of forecast and 15 May plus the evacuation necessary to attain the required reservoir level indicated by the latest tentative allocation.
- 3. From the date of the governing forecast each year through 31 July of that year herein designated the filling period, the reservoir shall be operated in such a manner that

the reservoir content shown on the chart (Plate I) will be maintained but not be exceeded except when storage above those levels is required to limit the flows to 20,000 second-feet at Heise. When the forecasted runoff indicates a required storage capacity in excess of the total active storage capacity of the reservoir, releases in excess of 20,000 second-feet will be made as required but at rates not to exceed 30,000 second-feet, except as indicated in paragraph 4 below.

- 4. Whenever the pool shall have risen above elevation 5,620, the full reservoir level, due to an extraordinary excess of inflow over the maximum releases permitted under paragraph 1 or is expected to rise above that level within the next 48 hours, releases may be increased temporarily above those previously specified, so as to minimize the peak rate of release and to draw the reservoir down to the full reservoir level as rapidly as possible. However, the maximum rate of such extraordinary release shall not exceed the estimated maximum mean daily rate of inflow to the reservoir during the period when the reservoir level is above elevation 5,620.
- 5. All reservoir releases made as herein provided are subject to the condition that no releases shall be made at rates or in a manner that would be inconsistent with whatever operating rules and regulations are laid down by the Chief Engineer of the Bureau of Reclamation for the purpose of protecting the dam and reservoir from damage.

If operating experience indicates the desirability therefor, the Secretary of the Interior may, after consultation with the Secretary of the Army, modify from time to time the operating plan herein described with respect to the amount of space allocated to flood control each year on the basis of advance forecasts as to runoff, but no modification which would result in a substantial change in the control of floods herein stated to be the objective of the original operating plan shall be made without the concurrence of the Secretary of the Army. Revisions of the rules and regulations prescribed under the Flood Control Act of 1944 will be made by the Secretary of the Army if, in his judgment, these are requisite because of such modifications in flood control space allocations. Modifications in the operating plan not requiring the concurrence of the Secretary of the Army shall not be the occasion for a revision of the conclusions originally reached as to the flood control benefits to be realized from the original operating plan or of the formula adopted for the allocation of construction costs to flood control purposes.

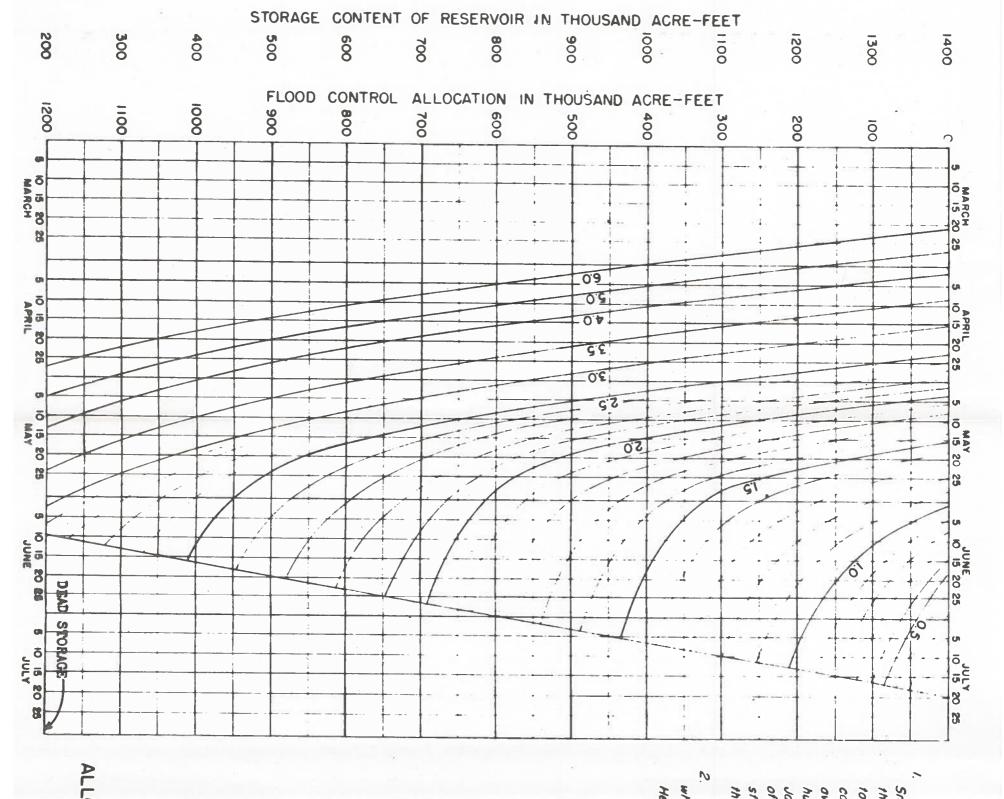
The reservoir content shows on the chart (Finth 1) will be maintained but put be expected sample when storage above oness levels is required by items to 20,000 record-inst ar 100 sec. Whin the four invested reading and additions a required above operator of the content of the section according to the reading of the reservoir relative in excuse of 30,000 records will be made as required but at rates not to exceed 30,000 records its paragraph 4 below.

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Parameters are anticipated flood run-off of Snake River at Heise in millons of acre-feet for the remainder of the season from any given date to July 31. The anticipated run-off is the fore-casted flow at Heise less the storage capacity available in Jackson Lake. A minimum of two hundred thousand acre-feet of storage space in Jackson Lake will be held vacant until May I of every year unless the forecast indicates that storage should begin earlier to insure filling that space.

NOTES:

Storage reservation based upon a release which would give a maximum regulated flow at Heise of twenty thousand second-feet.

UNITED STATES
DEPARTMENT OF THE INTERIOR
BUREAU OF RECLAMATION

PALISADES RESERVOIR PROJECT
IDAHO

ALLOCATION OF FLOOD CONTROL SPACE

BOISE, IDAHO OCTOBER 31, 1947

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APPENDIX B

TITLE 33--NAVIGATION AND NAVIGABLE WATERS

Chapter II--Corps of Engineers
Department of the Army

PART 208--FLOOD CONTROL REGULATIONS

PALISADES DAM AND RESERVOIR, SNAKE RIVER, IDAHO

Pursuant to the provisions of section 7 of the Act of Congress approved December 22, 1944 (58 Stat. 890; 33 U. S. C. 709), the following #208.91 is hereby prescribed to govern the use and operation of Palisades Dam and Reservoir on Snake River, Idaho, for flood control purposes.

- #208.91 Palisades Dam and Reservoir, Snake River, Idaho. The Bureau of Reclamation shall operate Palisades Dam and Reservoir in the interests of flood control as follows:
- (a) Storage space in Palisades Reservoir and Jackson Lake combined shall be kept available for flood control purposes in accordance with the Flood Control Storage Reservation Diagram currently in force. Not less than 75 percent of the total flood control space shall be made available in Palisades Reservoir.
- (b) Releases from Palisades Reservoir shall be restricted to quantities which will not cause downstream flows at the Heise gaging station to exceed 20,000 cubic feet per second, insofar as this control can be accomplished with combined reservoir capacity not exceeding 1,400,000 acre-feet in Palisades Reservoir and Jackson Lake.
- (c) When the total active capacity of the reservoir has been evacuated and when the forecasted runoff indicates that storage capacity in excess of 1,400,000 acre-feet may be required for Palisades Reservoir and Jackson Lake combined to control the flows at Heise gaging station to 20,000 cubic feet per second, releases in excess of 20,000 cubic feet per second prior to June 1 will be planned on the basis of the following rule curve:

	31 forecasted volume acre-feet):	Required discharge (c.f.s.)
Less than	4,100,000	20,000
4,100,000		23,000
4,300,000		24,000
4,600,000		25,000
4,900,000		26,000
5,300,000		27,000
5,600,000		28,000
6,000,000		29,000
6,300,000	or larger	30,000

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m l}$ Applicable only when exceeded by natural inflow.

- (d) When the forecasted runoff for the period June 1 through July 31 exceeds 2,500,000 acre-feet, and when, after June 1, the available space is not within 10,000 acre-feet of the space required by the Flood Control Storage Reservation Diagram currently in force, the releases from the reservoir may be increased so that the flow at Heise gaging station will exceed 20,000 c.f.s. up to a limit of 30,000 c.f.s. to the extent of 1,000 c.f.s. for each 5,000 acre-feet of deficient storage space, except that the release shall not be greater than the natural inflow. The change in discharge will be made in such manner as to minimize the adverse downstream effects.
- (e) In no case will releases be made which will cause the flow of Snake River at Heise gaging station to exceed 30,000 c.f.s. except as may be agreed upon by the Corps of Engineers and Bureau of Reclamation in the case of exceedingly large floods or as provided in paragraph (f) or (h) of this section.
- (f) The flood control regulations of the section are subject to temporary modification by the District Engineers, Corps of Engineers, if found necessary in time of emergency. Requests for and action on such modification may be made by any available means of communication, and the action taken by the District Engineer shall be confirmed in writing under date of the same day to the Office of the Regional Director of the Bureau of Reclamation in charge of the locality.
- (g) The Flood Control Storage Reservation Diagram currently in force as of the promulgation of this section is that dated May 12, 1958, File No. SN-902-1/1, and is on file in the Office of the Chief of Engineers, Department of the Army, Washington, D. C., and in the Office of the Commissioner, Bureau of Reclamation, Washington, D. C. Revisions of the Flood Control Storage Reservation Diagram may be developed from time to time as necessary by the Corps of Engineers and the Bureau of Reclamation. Each such revision shall be effective upon the date specified in the approval thereof by the Chief of Engineers and the Commissioner of Reclamation, and, from that date until replaced, shall be the Flood Control Storage Reservation Diagram currently in force for purposes of this section. Copies of the Flood Control Storage Reservation Diagram currently in force shall be kept on file in and may be obtained from the office of the District Engineer, Corps of Engineers, and the Regional Director, Bureau of Reclamation, in charge of the locality.
- (h) In the event that the reservoir level rises above elevation 5620 at the dam (top of spillway gates), care shall be taken that the maximum subsequent release from the reservoir does not exceed the corresponding rate of reservoir inflow.
- (i) Nothing in the regulations in this section shall be construed to require dangerously rapid changes in magnitude of releases, or that releases be made at rates or in a manner that would be inconsistent with requirements for protecting the dam and the reservoir from major damage.

- (j) The Bureau of Reclamation shall currently procure basic hydrologic data, make determinations of required flood control reservation from the Flood Control Storage Reservation Diagram currently in force and make calculations of permissible releases from the reservoir as are required to accomplish the flood control objectives prescribed in this section.
- (k) The Bureau of Reclamation shall keep the District Engineer, Corps of Engineers, Department of the Army, in charge of the locality, currently advised of hydrologic data and other operating criteria which affect the schedule of operation. Also, the Bureau of Reclamation shall keep the Watermaster, Water District No. 36, acting for the Department of Reclamation, State of Idaho, currently advised of reservoir releases.

(Regs., May 12, 1958, ENGWE) (Sec. 7, 58 Stat. 890; 33 U. S. C. 709)

(SEAL)

HERBERT M. JONES
Major General, U. S. Army,
The Adjutant General

(F. R. Doc. 58-4387; Filed, June 10, 1958; 8:45 a.m.)

Copies from Federal Register dated 11 June 1958

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APPENDIX C

FORECASTS OF RUNOFF - SNAKE RIVER AT HEISE 1955 Forecast Study - Upper Snake River Revised

January through July forecasts of "Inflow to Jackson Lake" and the "Inflow Between Moran and Heise" are determined from two groups of equations: (1) An early set, with precipitation as the primary forecasting parameter to be used before snow data become available for forecasts on January 1, February 1, and March 1, 1/ and (2) a later set of equations with the snow variable as the primary forecasting parameter to be used for April 1, May 1, June 1, and July 1 forecasts.

It should be noted that each forecast equation was derived from information available on the latest date shown in the subtitle. Forecasts for the earlier dates are obtained by substituting long-term average values for unavailable information.

The forecast of the Snake River at Heise is the sum of forecasts of inflow to Jackson Lake and the inflow between Moran and Heise.

Forecast of Inflow to Jackson Lake

January and February Forecast Equation (F55-2)

 $Y = 26.36X_1 + 66.43X_2 - 15.21X_3 + 205.99$

X₁ = Accumulated precipitation for September and October in inches, taken as average of measurements at Moran and Snake River.

^{1/} The inflow to Jackson Lake forecast on March 1 is an exception, since the April equation is used on March 1 by converting March 1 snow measurements to April 1 snow and substituting additional long-term averages where necessary.

- X₂ = Accumulated precipitation for November, December and January in inches, taken as average of measurements at Moran and Snake River.
- X_3 = The average variation of daily maximum temperatures above 35° at Moran for the preceding month of December measured in average degree days.
- Y = Forecast of inflow to Jackson Lake in 1,000 acre-feet for January 1 July 31. February 1 July 31 inflow forecast obtained by deducting recorded January inflow.

March, April, May, June, July Forecast Equation (A55-1) (Inflow to Jackson Lake)

- $Y = 21.51X_1 + 13.40X_2 + 34.90X_3 1.20X_4 66.84$
- X₁ = Snow water content on April 1 in inches taken as the average measured at Aster Creek, Coulter Creek, Glade Creek, Huckleberry Divide and Lewis Lake Divide. (On March 1 use March 1 snow water content plus 3.75 inches)
- X₂ = Accumulated precipitation at Snake River for period September through December, minus October through March inflow to Jackson Lake measured in inches. (Note: 1" over watershed = 43,520 acre-feet.) On March 1 use long-term average inflow for March.
- X₃ = The average of precipitation stations Moran and Snake River for April + 2/3 May + 1/3 June measured in inches. Use long-term average figures when current data not available. On March 1 and April 1 use 4.01 inches. (April = 1.93" 2/3 May = 1.38" and 1/3 June = 0.70")
- X₄ = December plus March maximum temperatures above 35° at Moran in average degree days. On March 1 use long-term average for March of 4.34.
- Y = Forecast of inflow to Jackson Lake in 1,000 acre-feet for April 1-July 31. Add average flow for March to obtain March 1-July 31 forecast of volume.

Forecast of Inflow Between Moran and Heise

January, February, and March Forecast Equation (M55-2)

 $Y = 246.96X_1 + 198.88X_2 - 121.96X_3 + 1017.40$

- X₁ = Accumulated precipitation for October, November and December in inches, taken as the average of measurements at Bedford, Jackson, Moran and Snake River, minus the runoff between Moran and Heise for October through December, measured in inches. 1¹¹ over the watershed = 262,613 acre-feet.
- X₂ = Accumulated precipitation for January and February in inches, taken as the average of measurements at Bedford, Jackson, Moran, and Snake River. Use 2.45 as average of 4 stations for January and 2.25 for February.
- X₃ = Average variation of daily maximum temperatures above 35^o at Moran for the preceding December in average degree days.
- Y = Forecast of inflow between Moran and Heise in 1,000 acre-feet for the period January 1-July 31, inclusive. (Forecasts of inflow for any date after January 1 estimated by subtracting actual flows.)

April, May, June, July Forecast Equation (A55-1) (Between Moran and Heise)

- $Y = 115.54x_1 + 15.04x_2 + 50.35x_3 + 19.43x_4 25.92x_5 + 321.3$
- X₁ = Snow water content on April 1 in inches taken as average measured at Togwotee Pass, Turpin Meadows, Yellowjacket, East Rim Divide, Blackrock and Four Mile Meadows.
- X₂ = Snow water content on April 1 in inches taken as average measured at Afton Ranger Station, CCC Camp, Cottonwood Lake, Deadman Ranch and Grover Park Divide.
- X₃ = Accumulated precipitation for October, November, and December taken as the average of measurements for Grover 2S, Bedford, Jackson, and Moran, minus 1/5 (November through March runoff between Moran and Heise) measured in inches. (1" over the watershed = 262,613 acre-feet.)
- X₄ = April + 2/3 May + 1/3 June precipitation in inches taken as
 the average of measurements at Bedford, Jackson and Moran.
 On April 1 use 3.39 inches. (April = 1.46, 2/3 May = 1.25",
 1/3 June = .69")
- X₅ = The average variation of daily maximum temperatures above 35° at Moran for the preceding December and March measured in average degree days.
- Y = Forecast of inflow between Moran and Heise in 1,000 acre-feet for the period April 1-July 31, inclusive.

- A; * Accessioned precipitation for October, nowember and Impendors
 In inches, collenses the everage of mestaurements of Bedford,
 Jackson, Nictus and Hoaks Livit, wings the runoff between
 Hurbs and Helps for October through December, setsuated in
 Inches, I over the valuation = 102,613 accellent.
- X2 = Actionships of practical for Lemmary and February in Indiana, taken on the average of emmetarables at Bodford, Jackson, borne, one Smake Siver. See 2,55 as average of 6 erations for Jacobry and 2,25 for Sebruary.
- To "Ot sworts entrancement minister within to continue against " of a
- ? Porseast of inflow actions Mozen and Hotes in 1,800 acre-field for the parted January 1-July 31, including. (Posiciants of inflow for any data after January 1 estimated by subtracting action flows.)

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- T 115.50x; 15.00x; 10.25x, 15.00x; 15.52x; 12.51.3
- X. = Show Water conjugation April 1 in inches taken as everage measured at Togotten Priss, Zurpin Headows, Vallenfacker, Lent Ein Divide, Blackrook and From Mile Headows.
- Ny Room water content on April I am Inches taken at appeage mineraped at Afton Roomer Station, GCC Camp, Cottonwood Lake, Dominan Rooms Not Drovet Park Divide.
- X; Accomplicat precipitation for October, November, and Decomber union as the average of remandrate for Grover St. Saufots, Septential, Septential,
 - At the state of members of members of medical inches them as the members of m
- A. The sworten variation of daily conjum comparators above 35° at Moren for the preceding December and Herch conserved in awareng degrae days.
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TABLE C-1

FORECAST RESULTS

Snake R. Near Heise, Idaho Snake R. at Moran, Wyoming

	May - July Volumes *				May - July Volumes *			
Date	Forecast	Actual	Forecast Error	Date	Forecast	Actual	Forecast Error	
1928 29 1930 31 32 33 34 1935 36 37 38 39 1940 41 42 43 44 1945 46 47 48 49 1950 51 52 53 54	3645 2473 1844 1282 2746 2546 1271 2613 3468 2447 2997 1740 2292 2125 4087 2042 2651 2446 3024 2717 3249 3586 3352 2658 3175	3793 2355 2143 1264 2942 2358 1173 2605 3425 2192 3145 2175 1769 1961 2320 3909 2085 2781 2742 3082 2864 2832 3730 3607 3286 2631 3076	-148 +118 -299 + 18 -196 +188 + 98 + 43 +255 -148 +112 - 29 +331 -195 +178 - 130 -296 - 58 -147 +1417 -148 - 21 + 66 + 27 + 99	1928 29 1930 31 32 33 34 1935 36 37 38 39 1940 42 43 44 1945 49 1950 51 52 53 54	855 569 538 361 791 716 355 738 890 720 846 698 619 574 6346 846 710 811 830 736 872	984 578 493 344 718 620 346 654 758 816 576 543 570 993 628 809 736 783 809 661 838	-129 - 9 + 45 + 17 + 73 + 96 + 9 + 84 +131 +162 + 76 + 74 + 2 - 81 + 19 + 69 + 37 - 26 +128 - 19 + 47 - 73 + 55 + 34	

^{*} All values in 1000 A.F.

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