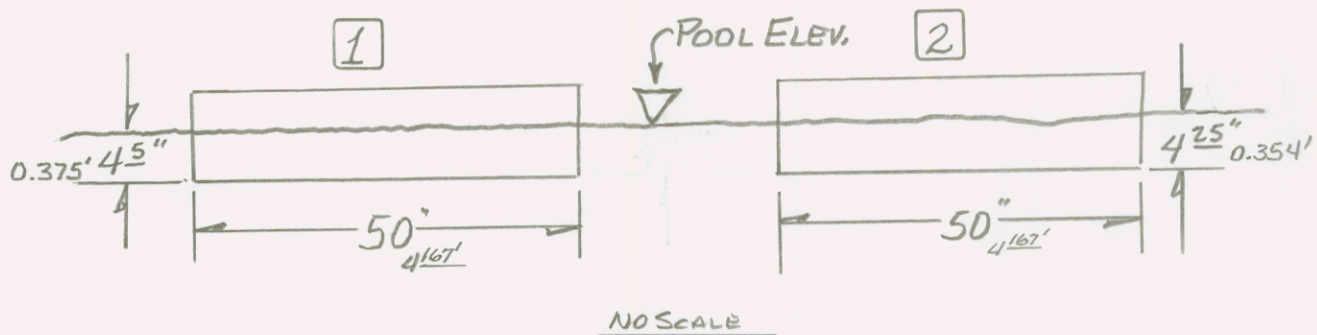


29-4178 STAT. CLAIM

I. STATE OF IDAHO - LAVA HOT SPRINGS FOUNDATION.

II. Q IS CLAIMED @ 30 cfs (NO KNOWN BASIS OR Q)

A. DISCHARGES OF PORTS (2) FROM LAVA HOT POND WERE MEASURED 11/14/02 BY A. RUBERRY AND C. BIRD. AS SHOWN IF FACING PORTS.



$$\boxed{1} \quad 4.167' \times 0.375' = 1.563' \text{ } \#$$

$$\text{AVG. } 1.52' \times 2 \text{ PORTS} = 3.04' \text{ } \#$$

$$\boxed{2} \quad 4.167' \times 0.354' = 1.475' \text{ } \#$$

VELOCITY MEASURED AT 1⁵⁰ CU FT / SEC.

$$3.04' \div 1.50 \text{ SEC.} = 2.027 \text{ cfs.}$$

$$2.027 \text{ cfs} \times 448 \text{ } \# \text{ GPM} = 909 \text{ } \# \text{ GPM} \times 3600 \text{ MIN/DAY} = 3.274 \text{ MILLION GAL/DAY}$$

PLUS 4" SUBMERGED PIPE $\approx$ 93K GPD

$$Q_0 = 3.3 \text{ MILLION GPD}$$

GPS DATA

663,557.27 $\longleftrightarrow$

170,722.15 $\updownarrow$

Table A7-2. Discharge of standard contracted rectangular weirs in ft³/sec. Shaded entries determined experimentally. All others computed from the formula $Q=3.33(L-0.2h_1)h_1^{1.5}$.

Head, h_1 ft	Weir Length, L , ft						
	0.5	1.0	1.5	2.0	3.0	4.0	5.0
0.18	0.122	0.286	0.435	0.584	0.882	1.18	1.48
0.19	0.132	0.307	0.467	0.627	0.948	1.27	1.59
0.20	0.142	0.329	0.500	0.672	1.02	1.36	1.70
0.21	0.152	0.350	0.534	0.718	1.09	1.45	1.82
0.22	0.162	0.373	0.568	0.764	1.16	1.55	1.94
0.23	0.173	0.395	0.604	0.812	1.23	1.64	2.06
0.24	0.184	0.419	0.639	0.860	1.30	1.74	2.18
0.25	0.195	0.442	0.676	0.909	1.38	1.84	2.31
0.26	---	0.466	0.712	0.959	1.45	1.95	2.44
0.27	---	0.490	0.750	1.01	1.53	2.05	2.57
0.28	---	0.514	0.788	1.06	1.61	2.16	2.70
0.29	---	---	---	---	---	---	---
0.30	---	---	---	---	---	---	---
0.31	---	0.539	0.827	1.11	1.69	2.26	2.84
0.32	---	0.564	0.866	1.17	1.77	2.37	2.98
0.33	---	0.590	0.905	1.22	1.85	2.48	3.11
0.34	---	0.615	0.945	1.28	1.94	2.60	3.26
0.35	---	0.658	0.986	1.33	2.02	2.71	3.40
0.36	---	---	---	---	---	---	---
0.37	---	0.686	1.03	1.39	2.11	2.83	3.54
0.38	---	0.714	1.07	1.44	2.19	2.94	3.69
0.39	---	0.743	1.11	1.50	2.28	3.06	3.84
0.40	---	0.772	1.15	1.56	2.37	3.18	3.99
0.41	---	0.801	1.20	1.62	2.46	3.30	4.14
0.42	---	0.830	1.24	1.68	2.55	3.43	4.30
0.43	---	0.860	1.28	1.74	2.64	3.55	4.46
0.44	---	0.890	1.33	1.80	2.74	3.68	4.61
0.45	---	0.920	1.37	1.86	2.83	3.80	4.77
0.46	---	0.950	1.42	1.92	2.93	3.93	4.94
0.47	---	0.981	1.46	1.98	3.02	4.06	5.10
0.48	---	1.01	1.51	2.05	3.12	4.19	5.26
0.49	---	1.04	1.55	2.11	3.22	4.32	5.43
0.50	---	1.08	1.60	2.17	3.31	4.46	5.60
0.51	---	1.11	1.65	2.24	3.41	4.59	5.77
0.52	---	---	---	---	---	---	---
0.53	---	---	---	---	---	---	---
0.54	---	---	---	---	---	---	---
0.55	---	---	---	---	---	---	---
0.56	---	---	---	---	---	---	---
0.57	---	---	---	---	---	---	---
0.58	---	---	---	---	---	---	---
0.59	---	---	---	---	---	---	---
0.60	---	---	---	---	---	---	---

Table A7-2 [continued]. Discharge of standard contracted rectangular weirs in ft³/sec. Shaded entries determined experimentally. All others computed from the formula $Q=3.33(L-0.2h_1)h_1^{1.5}$.

Head, h_1 ft	Weir Length, L , ft						
	2.0	3.0	4.0	5.0	6.0	7.0	8.0
0.61	2.98	4.57	6.15	7.74	9.33	10.9	12.5
0.62	3.05	4.68	6.30	7.93	9.55	11.2	12.8
0.63	3.12	4.79	6.45	8.12	9.78	11.4	13.1
0.64	3.19	4.90	6.60	8.31	10.0	11.7	13.4
0.65	3.26	5.01	6.75	8.50	10.2	12.0	13.7
0.66	3.34	5.12	6.91	8.69	10.5	12.3	14.0
0.67	3.41	5.23	7.06	8.89	10.7	12.5	14.2
0.68	3.58	5.35	7.22	9.08	10.9	12.8	14.5
0.69	3.66	5.46	7.37	9.28	11.2	13.1	14.8
0.70	3.74	5.58	7.53	9.48	11.4	13.4	15.1
0.71	3.82	5.69	7.69	9.68	11.7	13.7	15.4
0.72	3.90	5.81	7.84	9.88	11.9	13.9	15.7
0.73	3.98	5.93	8.00	10.1	12.2	14.2	16.0
0.74	4.06	6.05	8.17	10.3	12.4	14.5	16.3
0.75	4.14	6.16	8.33	10.5	12.7	14.8	16.6
0.76	4.22	6.28	8.49	10.7	12.9	15.1	16.9
0.77	4.30	6.40	8.65	10.9	13.2	15.4	17.2
0.78	4.38	6.52	8.82	11.1	13.4	15.7	17.5
0.79	4.46	6.65	8.98	11.3	13.7	16.0	17.8
0.80	4.54	6.77	9.15	11.5	13.9	16.3	18.1
0.81	4.62	6.89	9.32	11.7	14.2	16.6	18.4
0.82	4.70	7.01	9.49	12.0	14.4	16.9	18.8
0.83	4.78	7.14	9.65	12.2	14.7	17.2	19.1
0.84	4.87	7.26	9.82	12.4	15.0	17.5	19.4
0.85	4.96	7.39	9.99	12.6	15.2	17.8	19.7
0.86	5.05	7.51	10.2	12.8	15.5	18.1	20.0
0.87	5.14	7.64	10.3	13.0	15.7	18.4	20.4
0.88	5.23	7.76	10.5	13.3	16.0	18.8	20.7
0.89	5.32	7.89	10.7	13.5	16.3	19.1	21.0
0.90	5.41	8.02	10.9	13.7	16.5	19.4	21.3
0.91	5.50	8.15	11.0	13.9	16.8	19.7	21.6
0.92	5.59	8.27	11.2	14.2	17.1	20.0	21.9
0.93	5.68	8.40	11.4	14.4	17.4	20.4	22.2
0.94	5.77	8.53	11.6	14.6	17.6	20.7	22.6
0.95	5.86	8.66	11.7	14.8	17.9	21.0	22.9
0.96	5.95	8.80	11.9	15.1	18.2	21.3	23.3
0.97	6.04	8.93	12.1	15.3	18.5	21.7	23.6
0.98	6.13	9.06	12.3	15.5	18.8	22.0	24.0
0.99	6.22	9.19	12.5	15.8	19.0	22.3	24.3
1.00	6.31	9.32	12.7	16.0	19.3	22.6	24.7
1.01	---	---	---	---	---	---	---
1.02	---	---	---	---	---	---	---
1.03	---	---	---	---	---	---	---
1.04	---	---	---	---	---	---	---
1.05	---	---	---	---	---	---	---